

Gas standards for climate and air quality monitoring

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Bureau
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↓ **P**oids et
↓ **M**esures



Outline

- Introduction to Air Quality and Greenhouse Gas Monitoring
- Methods for Gas Standard preparation and verification
- Static Gravimetric Methods (CH_4 and NO)
- Dynamic Methods (NO_2 and HCHO)
- Spectroscopic Methods including isotopologues (O_3 and FTIR)
- Manometric Methods (CO_2 and O_3)

Air Quality and Greenhouse Gases



Air Quality

| <i>Pollutant</i> | <i>Concentration</i> | <i>Averaging period</i> |
|-------------------------------------|-----------------------|---------------------------|
| Ozone | 60 nmol/mol | Maximum daily 8 hour mean |
| Sulphur dioxide (SO ₂) | 120 nmol/mol | 1 hour |
| | 45 nmol/mol | 24 hours |
| Nitrogen dioxide (NO ₂) | 100 nmol/mol | 1 hour |
| | 20 nmol/mol | 1 year |
| Carbon monoxide (CO) | 8 µmol/mol | Maximum daily 8 hour mean |
| Benzene | 1.5 nmol/mol | 1 year |
| Fine particles (PM _{2.5}) | 25 µg/m ³ | 1 year |
| PM ₁₀ | 50 µg/m ³ | 24 hours |
| | 40 µg/m ³ | 1 year |
| Lead (Pb) | 0.5 µg/m ³ | 1 year |

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Greenhouse Gases

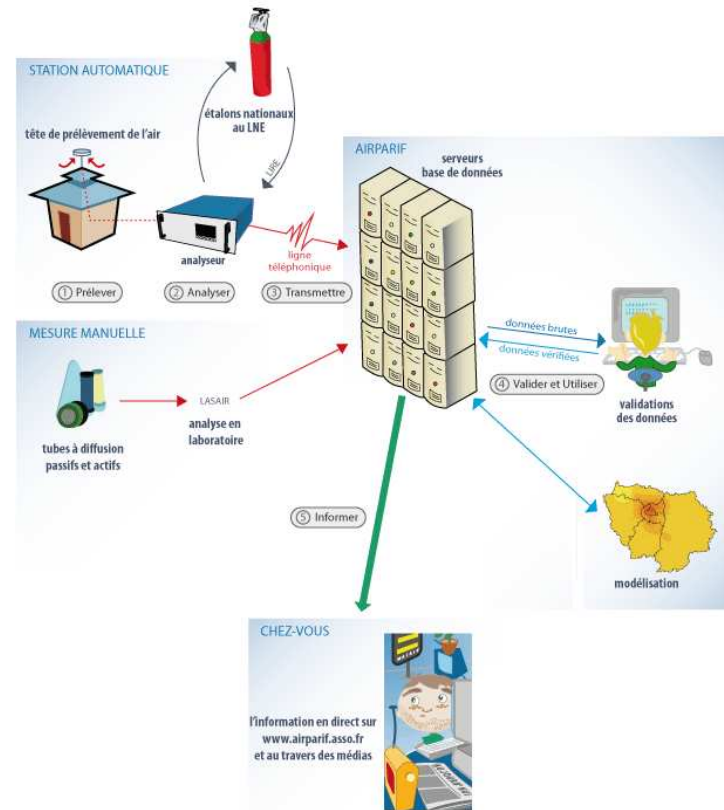


| GAS | Recent tropospheric concentration |
|--------------------------------------|-----------------------------------|
| Carbon dioxide (CO ₂) | 392.6 µmol/mol |
| Methane (CH ₄) | 1874 nmol/mol |
| Nitrous oxide (N ₂ O) | 324 nmol/mol |
| Tropospheric ozone (O ₃) | 34 nmol/mol |
| Halocarbons | (0.003 to 0.5) nmol/mol |

(Limit value concentrations)

Emission gases not included in list

Air Quality Monitoring Networks



The Essential Climate Variables

ECVs are either specific variables or groups of closely-related variables:

| | |
|--------------------|---|
| Atmospheric | <p>Surface: Air temperature, wind speed and direction, water vapour, pressure, precipitation, surface radiation budget</p> <p>Upper-air: Temperature, wind speed and direction, water vapour, cloud properties, earth radiation budget (including solar irradiance)</p> <p>Composition: Carbon dioxide, methane, and other long-lived greenhouse gases, ozone and aerosol, supported by their precursors</p> |
| Oceanic | <p>Surface: Sea-surface temperature, sea-surface salinity, sea level, sea state, sea ice, surface current, ocean colour, carbon dioxide partial pressure, ocean acidity, phytoplankton</p> <p>Sub-surface: Temperature, salinity, current, nutrients, carbon dioxide partial pressure, ocean acidity, oxygen, tracers</p> |
| Terrestrial | River discharge, water use, groundwater, lakes, snow cover, glaciers and ice caps, ice sheets, permafrost, albedo, land cover (including vegetation type), fraction of absorbed photosynthetically active radiation, leaf area index, above-ground biomass, soil carbon, fire disturbance, soil moisture |

For details see GCOS, 2010: Implementation plan for the global observing system for climate in support of the UNFCCC (2010 update) GCOS Rep. 138, 186 pp.



ICSU
International Council for Science



Table 1: Essential Climate Variables that are both currently feasible for global implementation and have a high impact on UNFCCC requirements

| Domain | Essential Climate Variables |
|--|---|
| Atmospheric (over land, sea and ice) | <p>Surface:⁸ Air temperature, Wind speed and direction, Water vapour, Pressure, Precipitation, Surface radiation budget.</p> <p>Upper-air:⁹ Temperature, Wind speed and direction, Water vapour, Cloud properties, Earth radiation budget (including solar irradiance).</p> <p>Composition: Carbon dioxide, Methane, and other long-lived greenhouse gases¹⁰, Ozone and Aerosol, supported by their precursors¹¹</p> |
| Oceanic | <p>Surface:¹² Sea-surface temperature, Sea-surface salinity, Sea level, Sea state, Sea ice, Surface current, Ocean colour, Carbon dioxide partial pressure, Ocean acidity, Phytoplankton.</p> <p>Sub-surface: Temperature, Salinity, Current, Nutrients, Carbon dioxide partial pressure, Ocean acidity, Oxygen, Tracers.</p> |
| Terrestrial | River discharge, Water use, Groundwater, Lakes, Snow cover, Glaciers and ice caps, Ice sheets, Permafrost, Albedo, Land cover (including vegetation type), Fraction of absorbed photosynthetically active radiation (FAPAR), Leaf area index (LAI), Above-ground biomass, Soil carbon, Fire disturbance, Soil moisture. |

⁸ Including measurements at standardized, but globally varying heights in close proximity to the surface.

⁹ Up to the stratopause.

¹⁰ Including N₂O, CFCs, HCFCs, HFCs, SF₆ and PFCs.

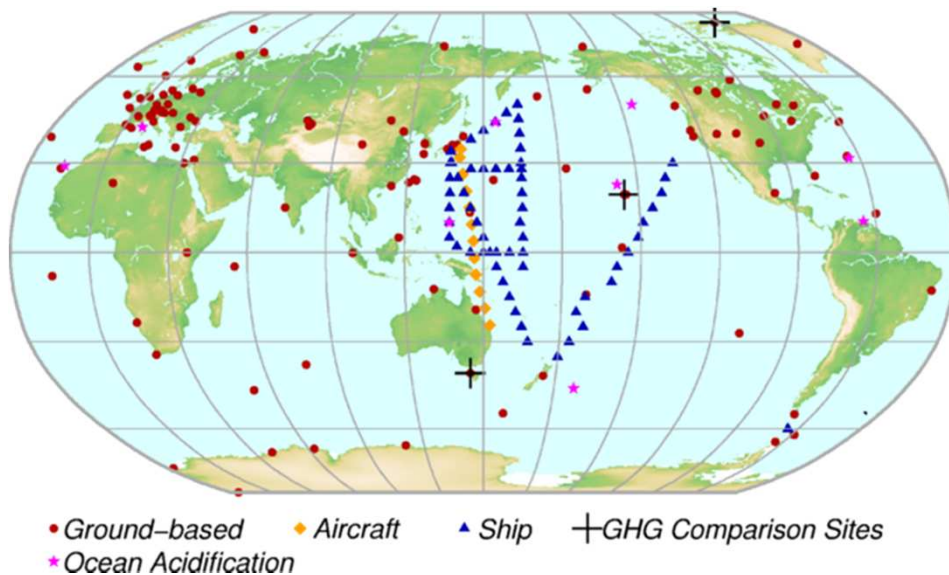
¹¹ In particular NO₂, SO₂, HCHO and CO.

¹² Including measurements within the surface mixed layer, usually within the upper 15 m.

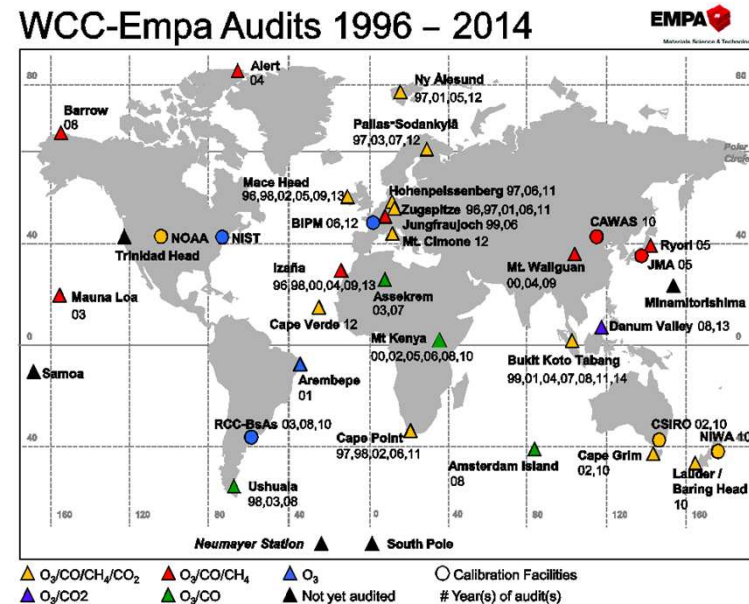
Greenhouse Gases: A Global View



WMO GAW GHG Network



WCC-Empa Audits 1996 – 2014



The network consists of 141, 123 and 49 fixed stations on the ground for CO₂, CH₄ and N₂O respectively. About 13%, 13% and 18% of the stations perform both discrete air sampling in “flasks” and continuous measurements of CO₂, CH₄ and N₂O, respectively.

Data Quality Objectives for GHGs



| Component | Compatibility goal | Extended compatibility goal | Range in unpolluted troposphere | Range covered by the WMO scale |
|---------------------------------------|---|-----------------------------|---|--------------------------------|
| CO₂ | ± 0.1 ppm (Northern hemisphere) ± 0.05 ppm (South. hemisphere) | ± 0.2 ppm | 360 - 450 ppm | 250 – 520 ppm |
| CH₄ | ± 2 ppb | ± 5 ppb | 1700 – 2100 ppb | 300 – 2600 ppb |
| CO | ± 2 ppb | ± 5 ppb | 30 – 300 ppb | 20 -500 ppb |
| N₂O | ± 0.1 ppb | ± 0.3 ppb | 320 – 335 ppb | 260 – 370 ppb |
| SF₆ | ± 0.02 ppt | ± 0.05 ppt | 6 – 10 ppt | 1.1 – 9.8 ppt |
| H₂ | ± 2 ppb | ± 5 ppb | 450 – 600 ppb | 140 – 1200 ppb |
| δ¹³C-CO₂ | ± 0.01‰ | ± 0.1‰ | -7.5 to -9‰vs. VPDB | |
| δ¹⁸O-CO₂ | ± 0.05‰ | ± 0.1‰ | -2 to +2‰vs. VPDB | |
| Δ¹⁴C-CO₂ | ± 0.5‰ | ± 3‰ | 0-70‰ | |
| Δ¹⁴C-CH₄ | ± 0.5‰ | | 50-350‰ | |
| Δ¹⁴C-CO | ± 2 molecules cm ⁻³ | | 0-25 molecules cm ⁻³ | |
| δ¹³C-CH₄ | ± 0.02‰ | ± 0.2‰ | | |
| δD-CH₄ | ± 1‰ | ± 5‰ | | |
| O₂/N₂ | ± 2 per meg | ± 10 per meg | -250 to -800 per meg (vs. SIO scale) | |

Reviewed at GGMT-2013



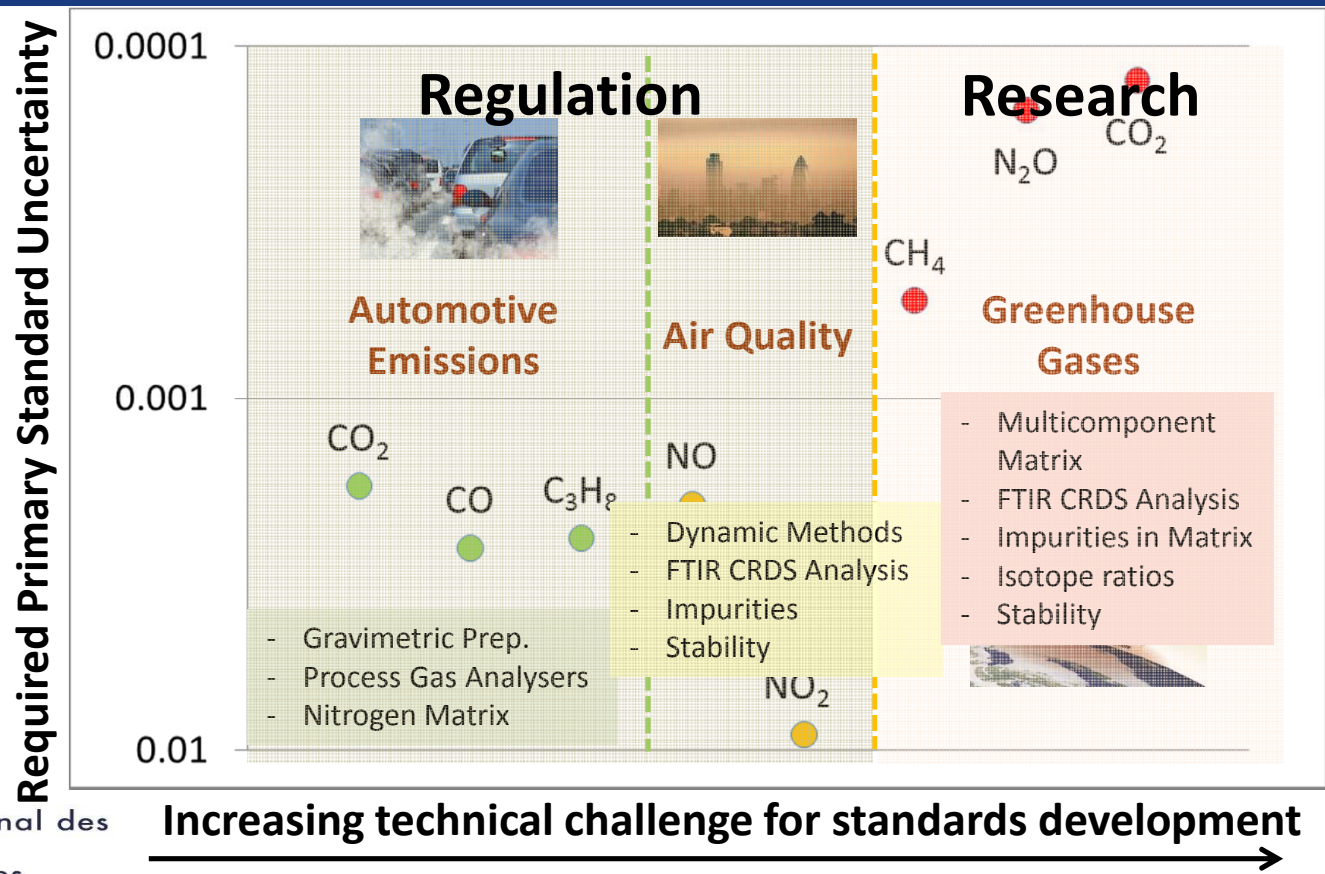
Target uncertainties for GHG primary standards

| Component | Nominal Mole fraction | Primary Standard: target standard uncertainty |
|------------------|-----------------------|---|
| CO ₂ | 400 μmol/mol | 0.025 μmol/mol |
| CH ₄ | 2000 nmol/mol | 0.5 nmol/mol |
| N ₂ O | 330 nmol/mol | 0.025 nmol/mol |

Based on primary standard contributing to less than 5% of measurement uncertainty for monitoring, based on most stringent data compatibility requirements

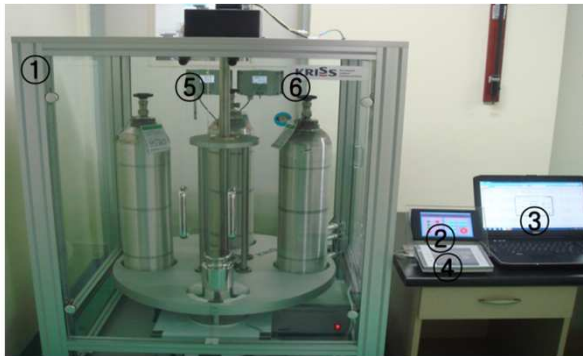
This means relative standard uncertainties:

Gas Standards in support of Regulation and Research

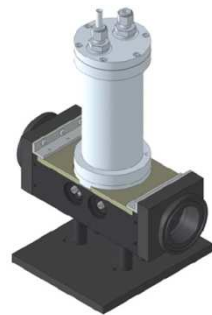
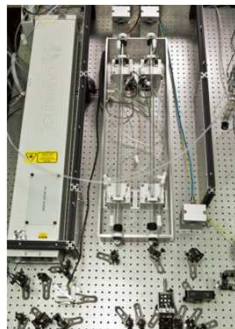
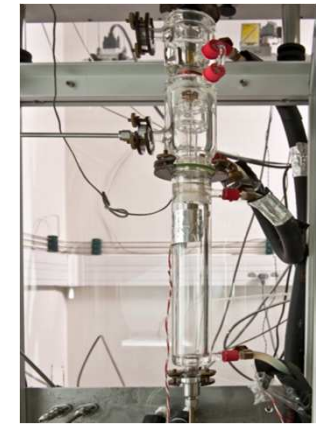


Methods for Gas Standard Preparation and Value Assignment

Static Gravimetry



Dynamic Methods



Spectroscopic Methods



Manometric Methods

Gas Standards: International documentary standards

- ISO TC158 Gas Analysis
- ISO 6142 : Gas Analysis – Preparation of calibration gas mixtures – Gravimetric method
- ISO 6143 : Gas Analysis – Comparison methods for determining and checking the composition of calibration gas mixtures

Preparation of Gas Standards (Static)

- **Purity Analysis of Gases; Impurity Analysis; purity = $1 - \sum x_i$**
GC(FID, TCD, ECD, AED, USD, DID, SCD, MSD)
Dedicated Analyzer(H_2 , O_2 , Ar, N_2 , CH_4 , CO, CO_2 , SO_2 , NO_x , H_2O , THC, CFCs, PFCs)
FTIR, Gas MS
- **Gravimetry, Micro-gravimetry;**
Top-loading Electronic Balance
(10 kg/1mg, 15 kg/1 mg, 23 kg/1 mg , 1 kg/0.01 mg, 22 g/1 μ g)
Substitution Method, Capillary Method

Calculation of Mixture Composition (ISO 6142)

$$x_i = \frac{\sum_{A=1}^P \left(\frac{x_{i,A} \cdot m_A}{\sum_{i=1}^n x_{i,A} \cdot M_i} \right)}{\sum_{A=1}^P \left(\frac{m_A}{\sum_{i=1}^n x_{i,A} \cdot M_i} \right)}$$

x_i is the mole fraction of component i in the resulting mixture

P is the total number of the parent gases

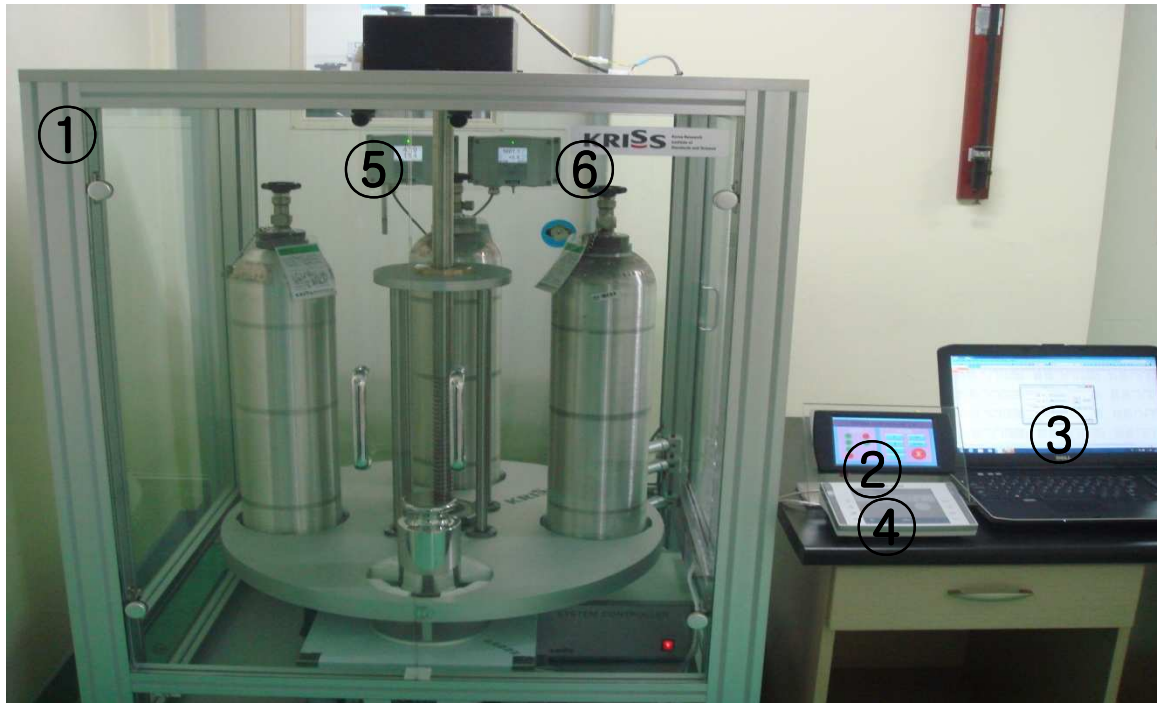
n is the total number of the parent gases

m_A is the mass of the parent gas A measured by weighing

M_i is the molar mass of component I

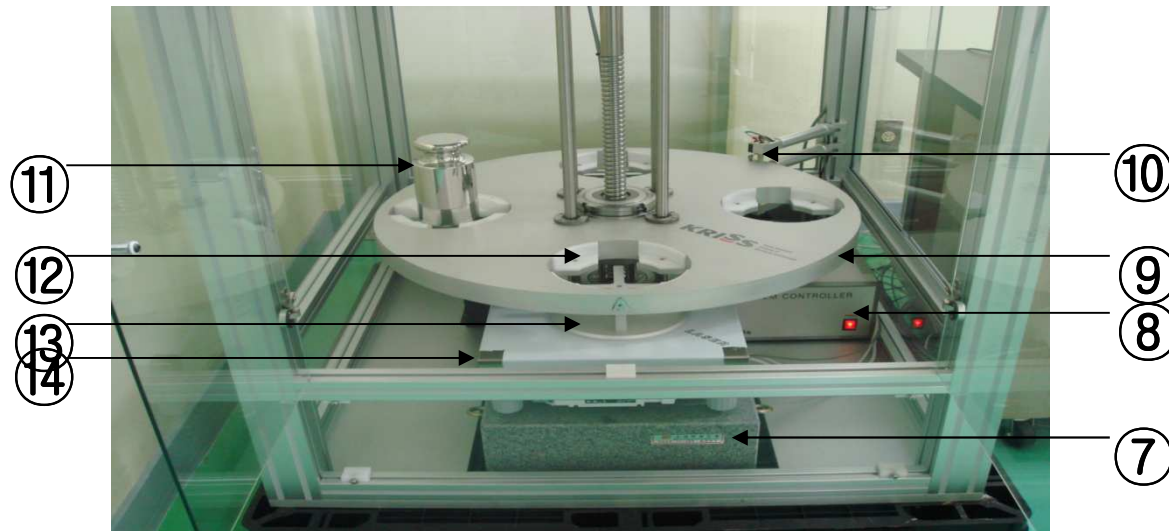
$x_{i,A}$ is the mole fraction i in the parent gas A

Automatic Gas Cylinder Weighing System (KRISS)



- ① Draft shield
- ② Manual controller
(LCD touch screen)
- ③ Computer
- ④ Balance display(LCD)
- ⑤ Humidity & Temp.
Transmitter
- ⑥ Barometer

Automatic Gas Cylinder Weighing System (KRISS)



⑦ Stone plate

⑧ System controller

⑨ Rotation plate

⑩ Upper & limit sensor

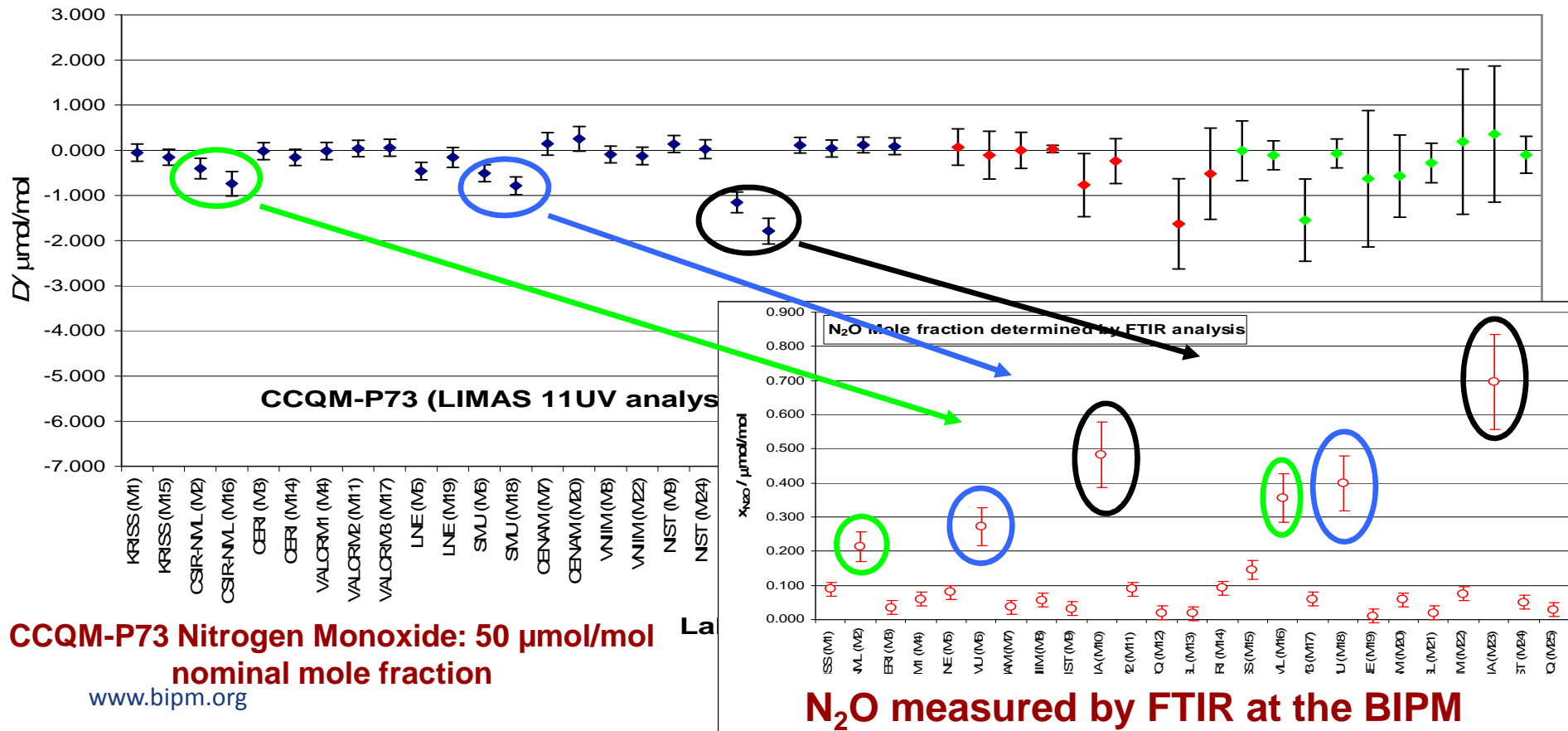
⑪ Mass(D)

⑫ Cylinder position(A, B, C)

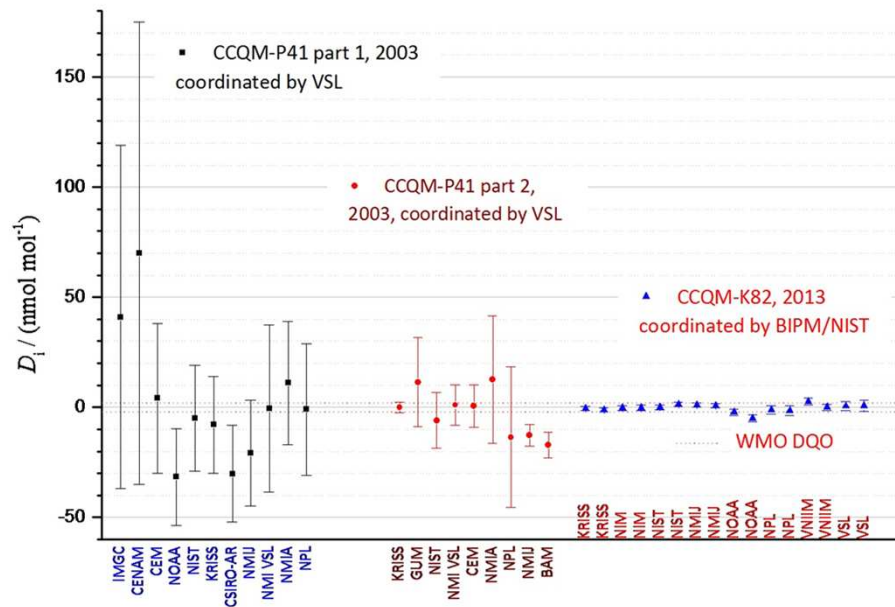
⑬ Cylinder support

⑭ Balance

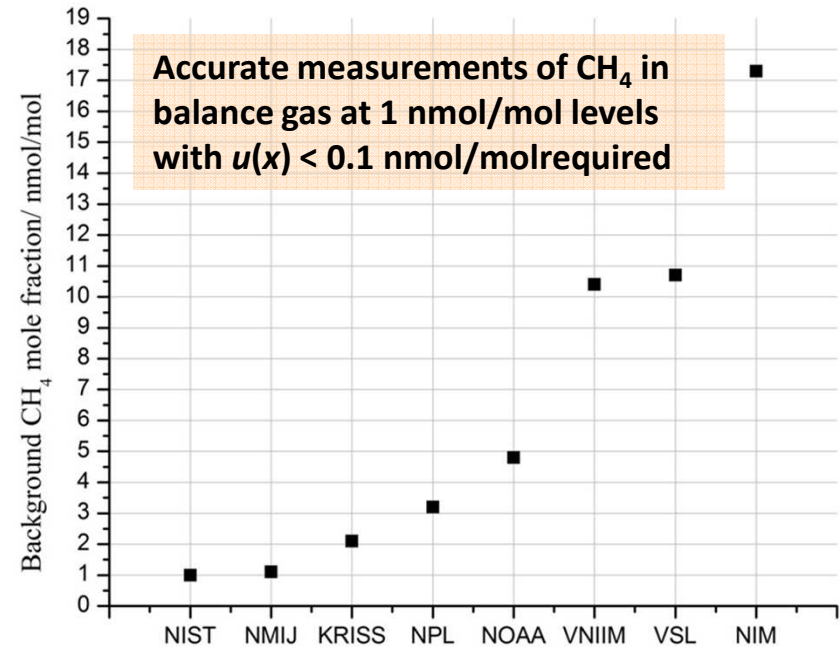
Equivalence of standards produced by Static Gravimetry (NO in N₂)



Equivalence of standards produced by Static Gravimetry (CH₄ in Air)



Methane in air nominal mole fraction 2000 nmol/mol



Trace CH₄ mole fractions in balance gas as reported by participating laboratories in CCQM-K82

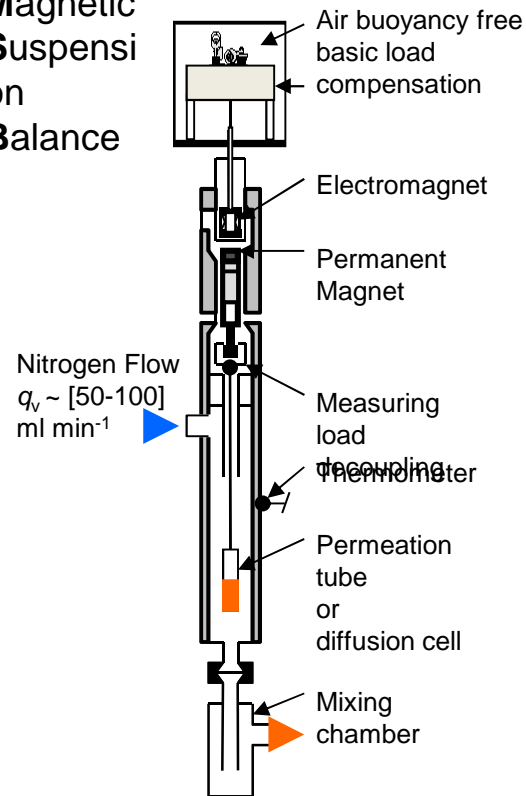
Dynamic gas standard generation



Magnetic Suspension Balance



Magnetic Suspension on Balance



Magnetic Suspension Balance:

- Mass load 20 g
- Resolution 2 μg
- Stability over 3 days $\sim 0.5 \mu\text{g}$

Measurement of the **mass** of the permeation tube emitting the analyte


Deduction of the **permeation rate** $q_m / (\text{ng min}^{-1})$
= mass loss per unit of time

$$q_m = \frac{dm}{dt}$$

And the amount of substance fraction

$$x_A = \frac{q_m V_m}{q_v M_A}$$

Generation of formaldehyde in nitrogen mixtures



Permeation tube at 110°C

$$\text{HO}-\left[\begin{array}{c} \text{H} \\ | \\ \text{C} \\ | \\ \text{H} \end{array} \right]_n-\text{H}$$

8-100

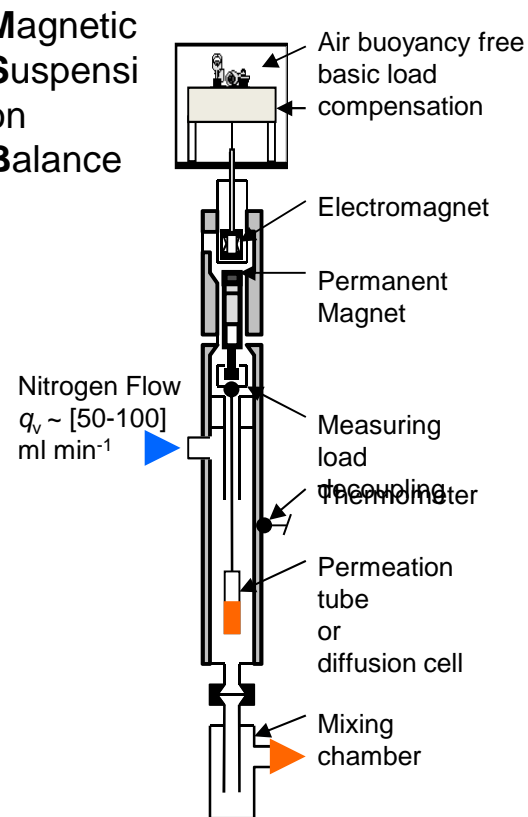

Paraformaldehyde

+ correction for co-emitted water

$$x_{\text{HCHO}} = \frac{q_m V_m}{q_v M_{\text{HCHO}}} - \frac{M_{\text{H}_2\text{O}}}{M_{\text{HCHO}}} x_{\text{H}_2\text{O}}$$

Water content measured by CRDS with/without permeation tube in the chamber. Typically 0.5%

Magnetic Suspension on Balance

Diffusion cell at 20°C

$$\begin{array}{c} \text{O} \\ / \quad \backslash \\ \text{H}-\text{C}-\text{H} \quad \text{H}-\text{C}-\text{H} \\ | \quad \quad | \\ \text{O} \quad \quad \text{O} \\ \backslash \quad / \\ \text{H} \\ | \\ \text{H} \end{array}$$

Trioxane

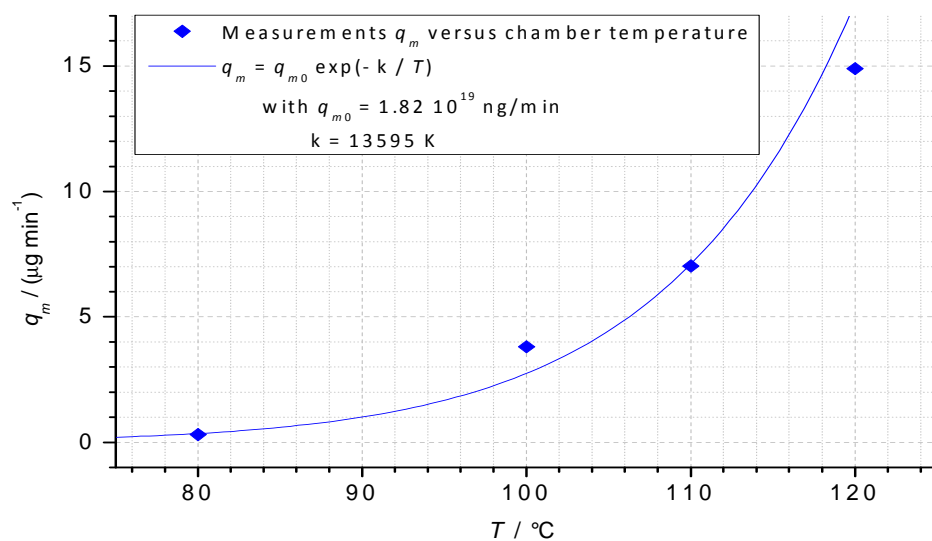
+ converter at 200°C

$$x_{\text{HCHO}} = \frac{3q_m V_m}{q_v M_{(\text{HCHO})_3}} \beta_{\text{conv}}$$

Conversion factor measured by FTIR with/without converter. 100% conversion with 0.1% uncertainty.

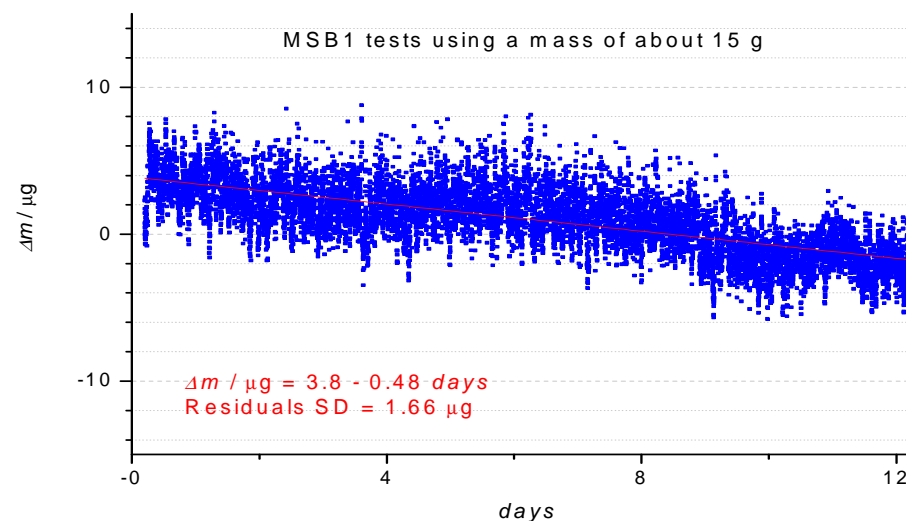
Choice of source temperature

Chamber temperature to be defined to reach the target analyte concentration....



Mass loss rate vs. gas chamber temperature study (paraformaldehyde source)

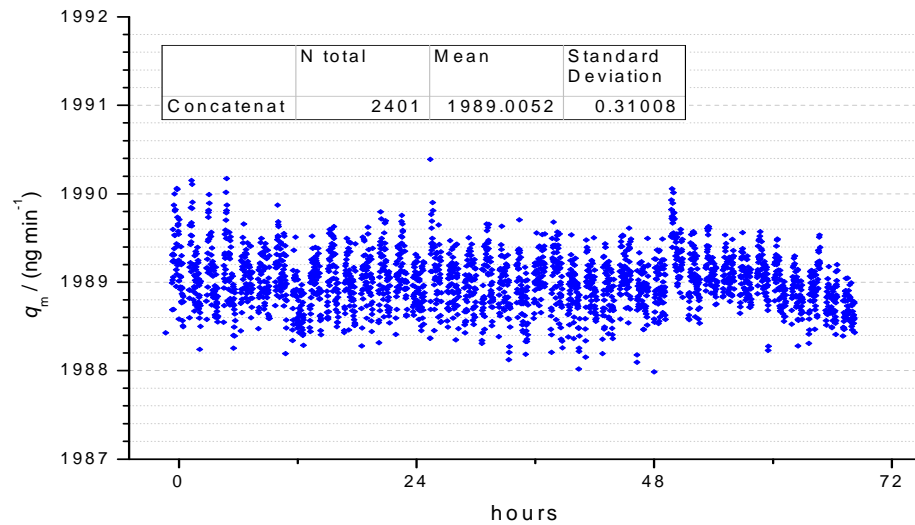
... and maintained within fixed limits



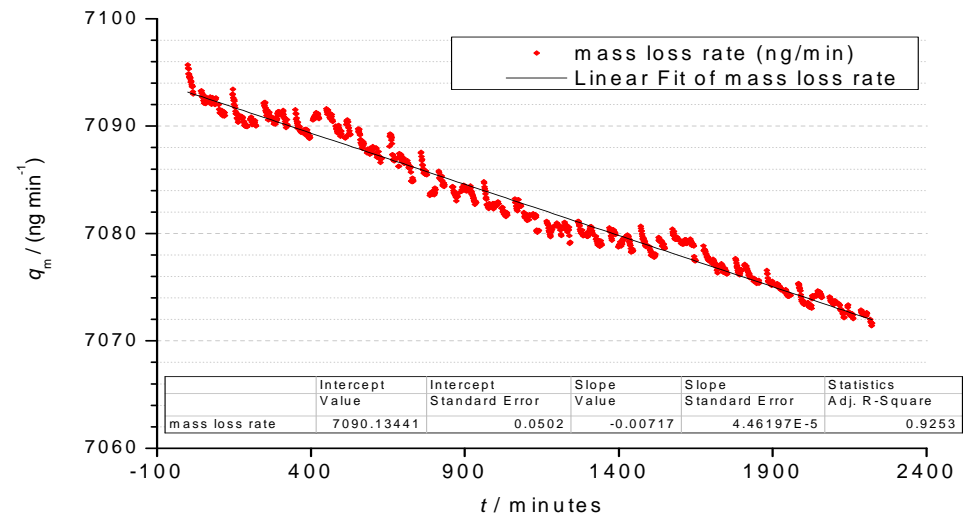
Target noise RSD < 3 µg
With temperature noise < 0.01 K

Mass loss rate analysis

q_m is almost never constant, even at constant temperature control



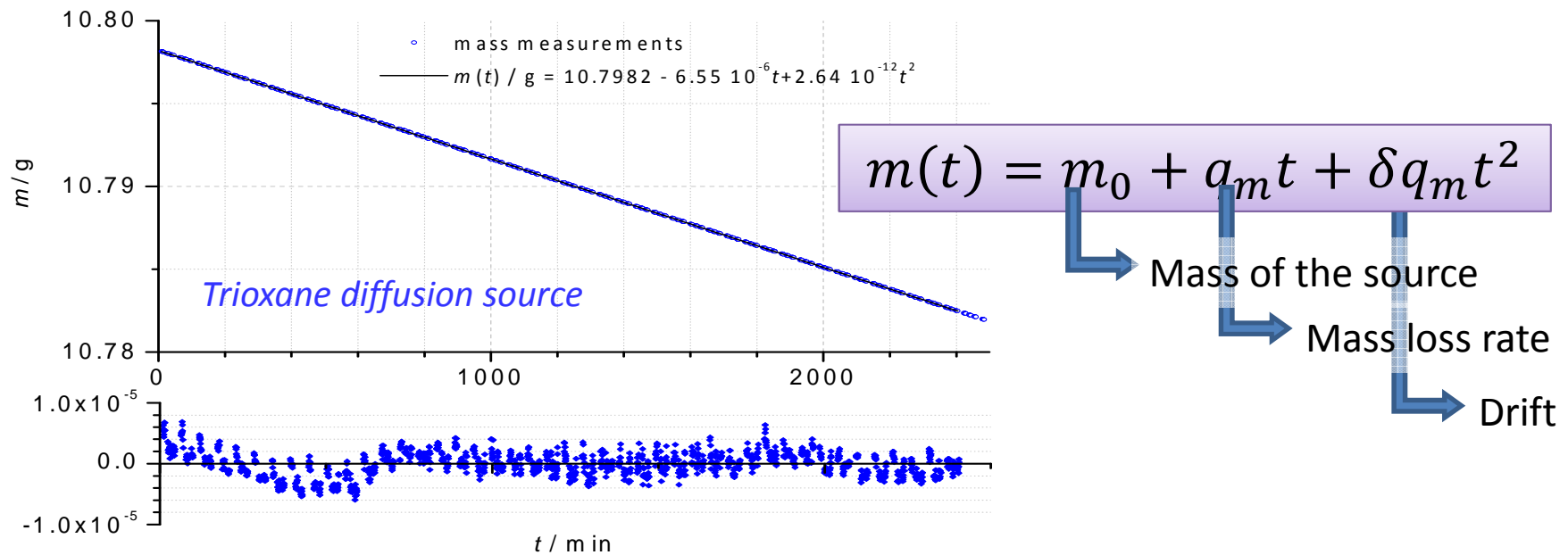
Trioxane diffusion source at 5°C
 Low values 1900 ng min⁻¹
 Slow drift
 Source duration > 1 year
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Paraformaldehyde permeation source at 110°C
 Large values 7000 ng min⁻¹
 Faster drift
 Source duration < 4 months

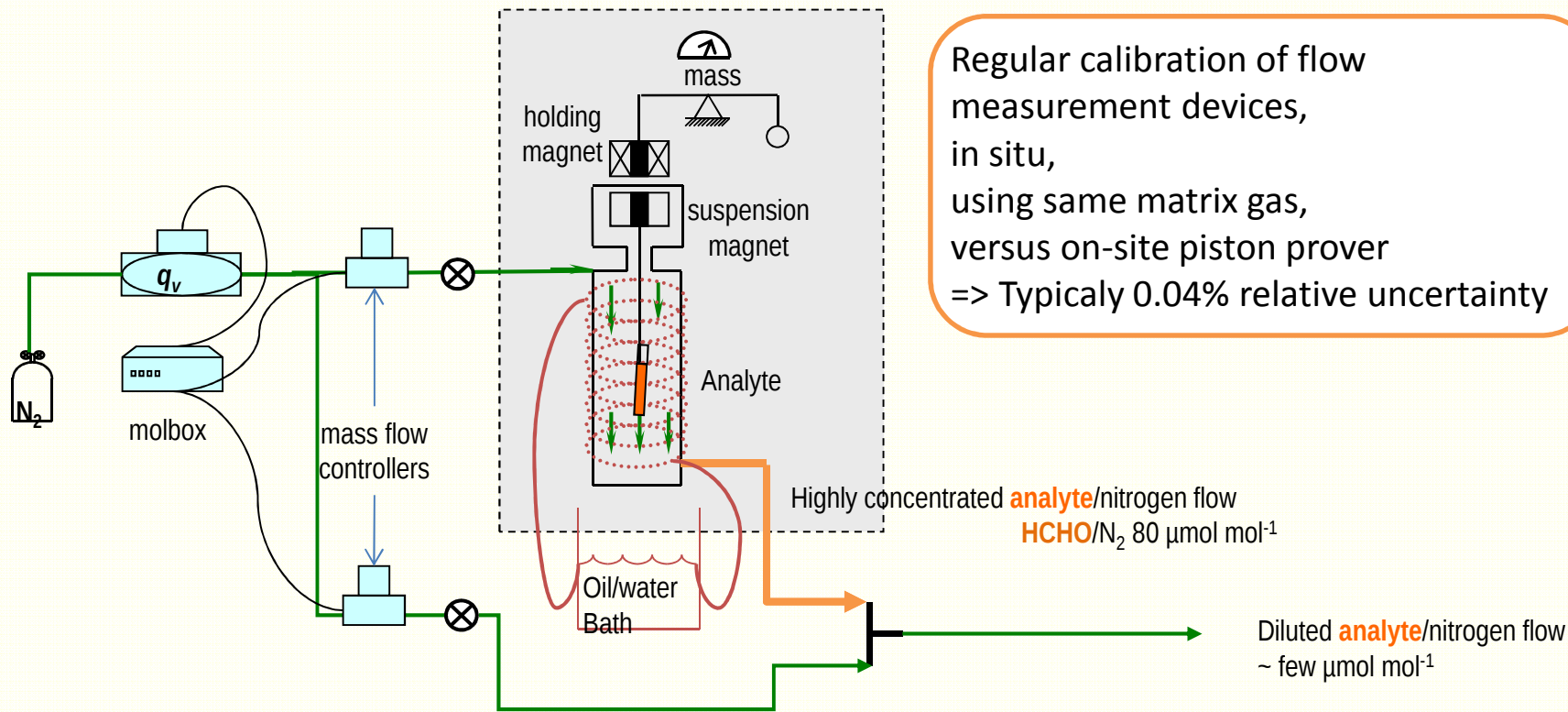
Choice of statistical analysis

Polynomial fit of mass continuous measurements during a typical analysis period



Target : RSD < 10 μ g in order to obtain typical relative uncertainty < 0.1%

Flow control & measurement



Regular calibration of flow measurement devices, in situ, using same matrix gas, versus on-site piston prover => Typically 0.04% relative uncertainty

Purity analysis

$$x_A = \frac{q_m V_m}{q_v M_A}$$

Analyte amount fraction **if pure**

$$x_A = \frac{q_m V_m}{q_v M} - \sum_i \frac{M_i x_i}{M_A} - \sum_j x_j \Rightarrow \text{Impurities from reaction with analyte}$$

↓
Impurities in the source

Contribution of impurities can be large!

| Analyte | Amount fraction / nmol mol ⁻¹ | Main impurity | Amount fraction / nmol mol ⁻¹ | Uncertainty contribution |
|------------------|--|------------------|--|--------------------------|
| NO ₂ | 8860 | HNO ₃ | 104 | 88.9% |
| HCHO | 2030 | H ₂ O | 12 | 79.5% |
| HNO ₃ | 456 | H ₂ O | 750 | 81.15% |

Purity analysis by FTIR

Fourier Transformed InfraRed spectrometer to quantify (infrared actives) impurities
 Calibration either with gravimetric standards or using molecular parameters

Database of spectroscopic parameters
 (**HITRAN** or PNNL or NIST library)

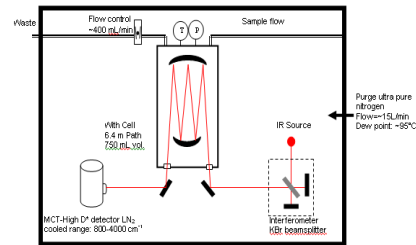
| | | | | | | | | | | | | |
|----|-------------|-----------|-----------|-------------|-----------|-----|---------|----|----|---|----|-----|
| 21 | 2290.645159 | 2.450E-25 | 7.574E-02 | 0.0877.1204 | 3245.3348 | .75 | .000000 | 56 | 18 | Q | 3 | 455 |
| 2 | 2 | 1 | | | | | | | | | | |
| 22 | 2290.662655 | 6.192E-24 | 4.750E-02 | 0.0670.0772 | 2073.5014 | .78 | .000000 | 25 | 5 | R | 42 | 455 |
| 2 | 2 | 1 | | | | | | | | | | |
| 23 | 2290.666003 | 9.230E-24 | 4.987E-02 | 0.0713.0966 | 1495.8581 | .76 | .000000 | 24 | 4 | P | 21 | 455 |
| 2 | 2 | 1 | | | | | | | | | | |

Synthetic calibration – uncertainty driven by database
 5-10 %

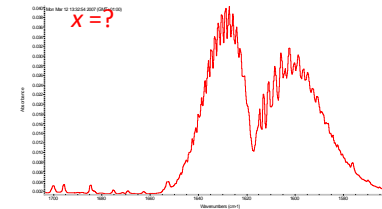


Gas standard calibration –
 uncertainty driven by gravimetry
 < 1%

FTIR



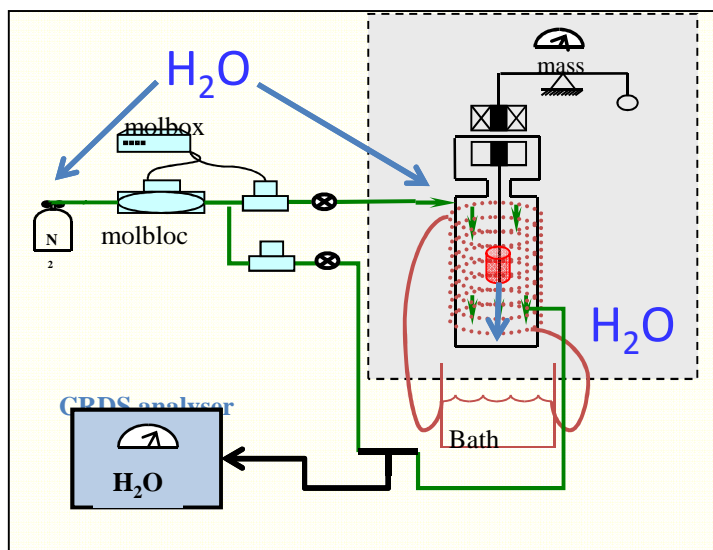
Measured spectrum



Water as impurity

FTIR : not appropriate to analyse trace water (large cell, leaks, ...)

CRDS : specific analyser, good a trace levels



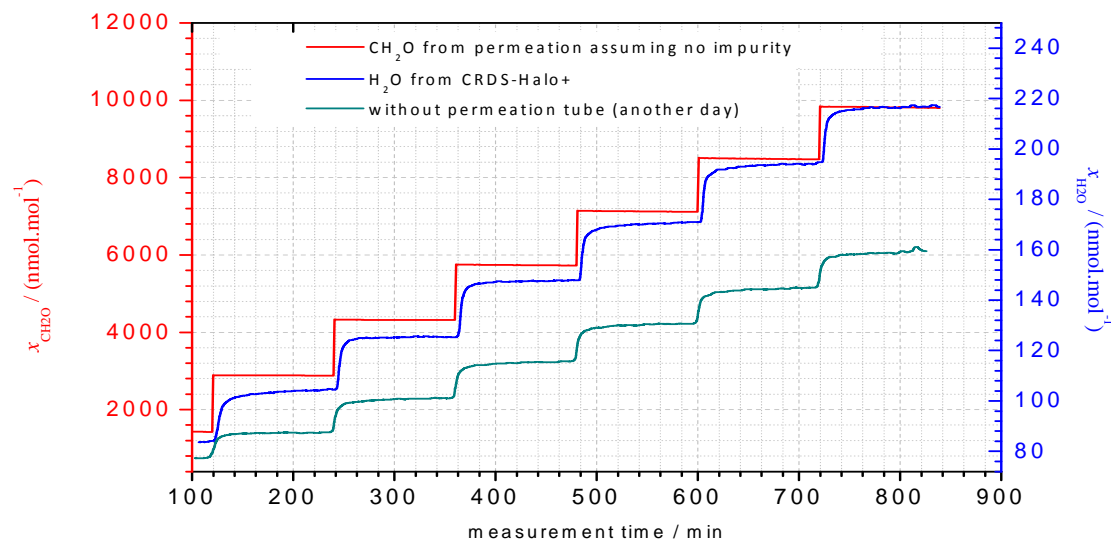
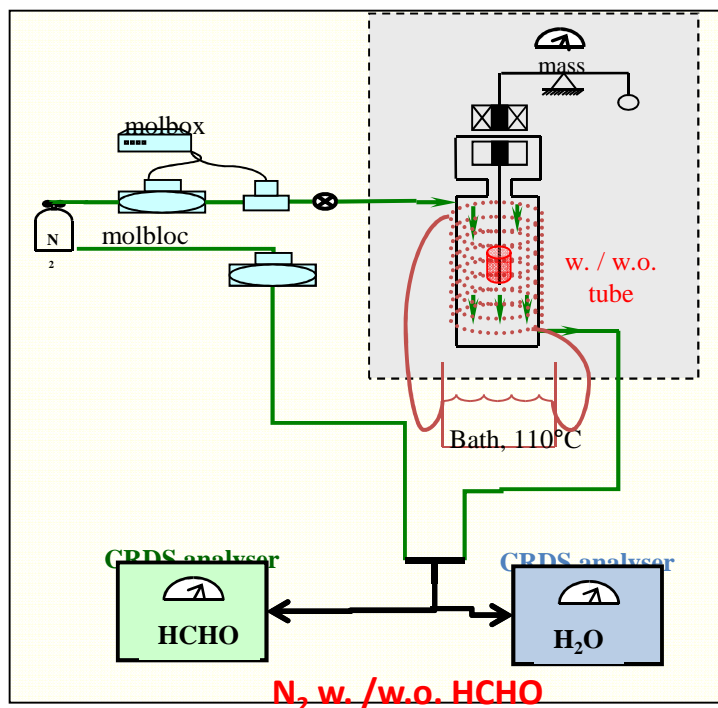
Specific precautions:

- Stainless steel chamber
- Coated tubes
- Dry nitrogen as matrix
- Calibration of water CRDS analyser
~ 5% uncertainty



Water quantification in HCHO from paraformaldehyde

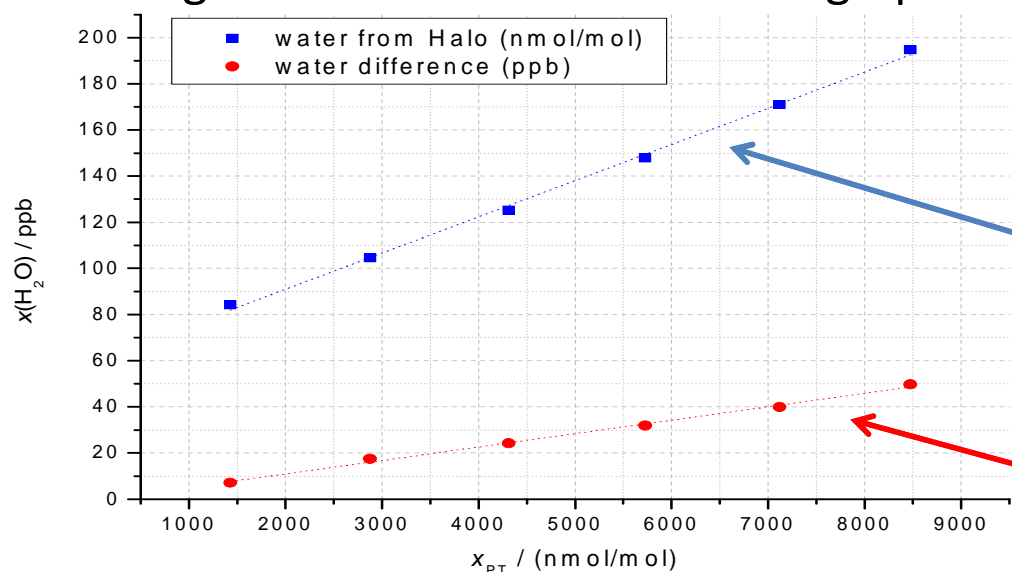
Distinction to be made between water from the source / water from the system



Evidence of lower H₂O without tube

Water quantification in HCHO from paraformaldehyde

Linear regression of the data from the graph:

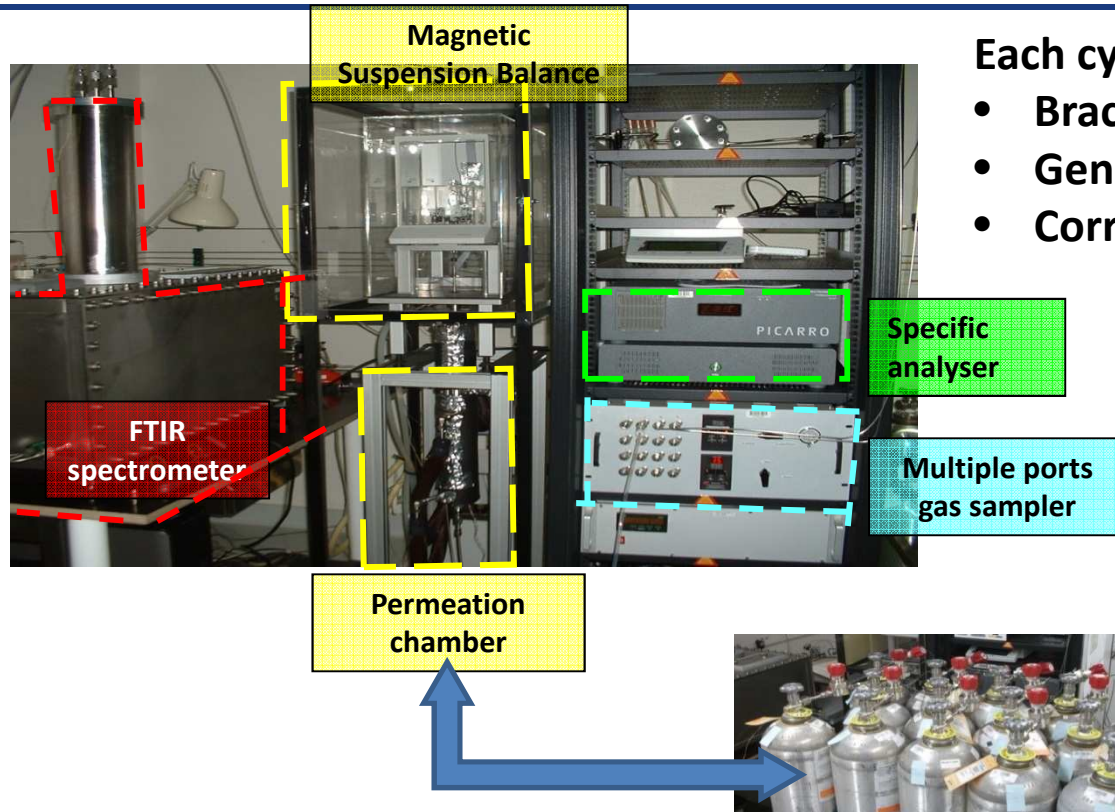


Total water mole fraction measured equivalent to 1.5% of mass loss

0.6% of mass loss is water permeating from Paraformaldehyde tube

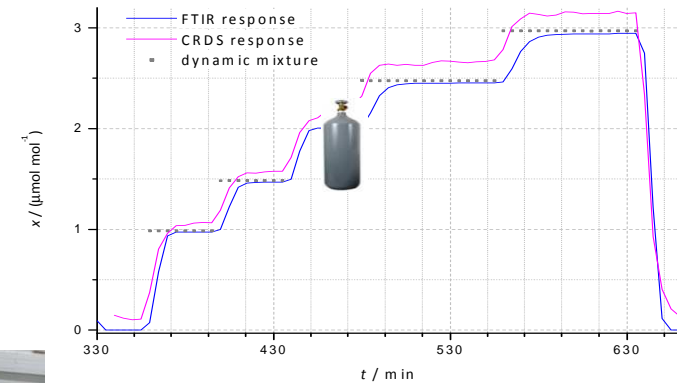
| | Intercept Value | Intercept Standard Error | Slope Value | Slope Standard Error | Statistics Adj. R-Square |
|------------------|-----------------|--------------------------|-------------|----------------------|--------------------------|
| water from Halo | 59.60407 | 1.89608 | 0.01568 | 3.42202E-4 | 0.99762 |
| water difference | -0.68917 | 1.01861 | 0.00582 | 1.83837E-4 | 0.99504 |

Value assignment of mixtures in cylinder



Each cylinder is value assigned

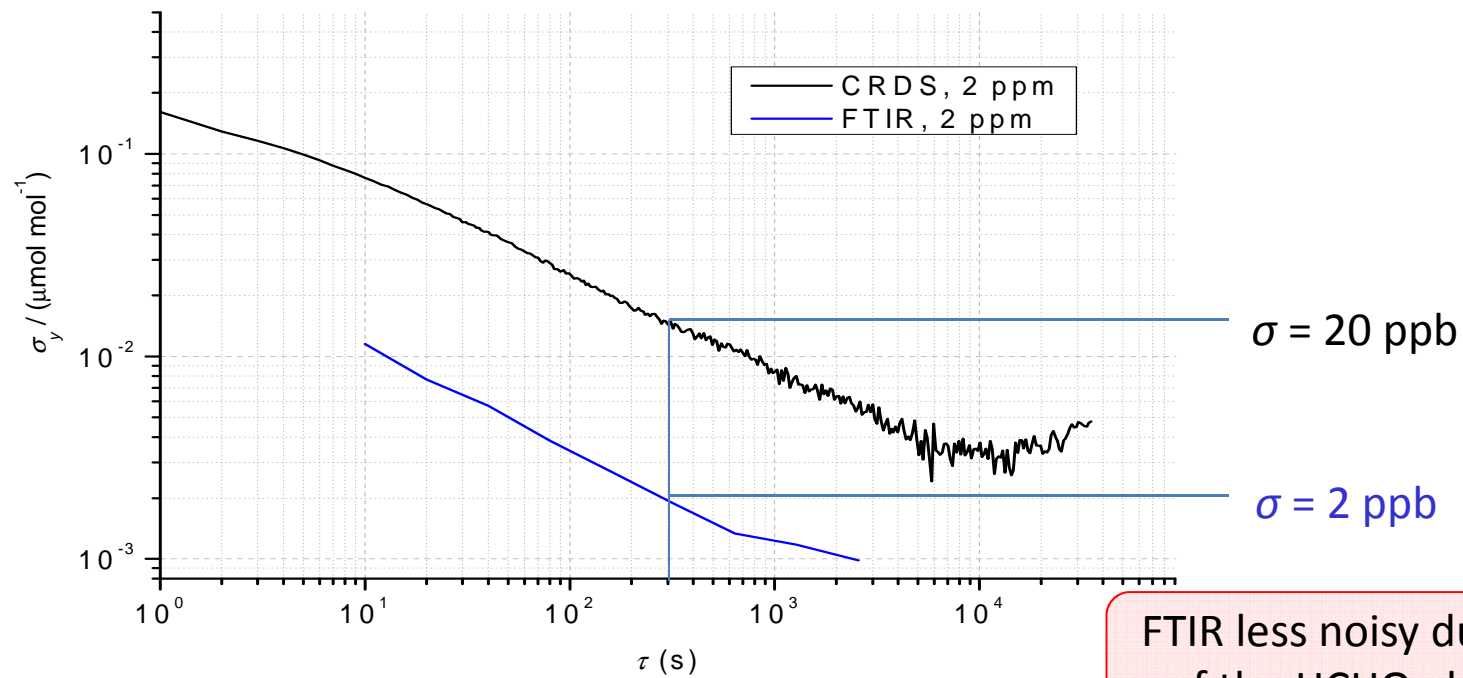
- Bracketing with 4 dynamic values
- Generalised Least-Square fit
- Correlation between dynamic mixtures



One cylinder value assignment sequence (~ 300 min)

Stability of analytical instruments

FTIR and CRDS stability compared on 2 $\mu\text{mol mol}^{-1}$ of formaldehyde/nitrogen



FTIR less noisy due to the choice of the HCHO absorption band

Uncertainty of dynamic calibration gas

HCHO from paraformaldehyde

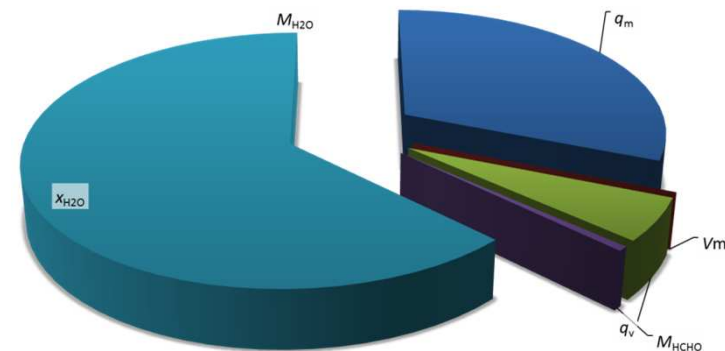
| Quantity | Value | unit | Standard relative uncertainty |
|--------------------------|---------|------------------------|-------------------------------|
| q_m | 7000.00 | ng min ⁻¹ | 1.21×10^{-3} |
| V_m | 22.4037 | L mol ⁻¹ | 1.52×10^{-5} |
| q_v | 2.5 | L min ⁻¹ | 5.12×10^{-4} |
| M_{HCHO} | 30.026 | g mol ⁻¹ | 6.66×10^{-5} |
| $x_{\text{H}_2\text{O}}$ | 12.00 | nmol mol ⁻¹ | 5.00×10^{-1} |
| $M_{\text{H}_2\text{O}}$ | 18.053 | g mol ⁻¹ | 2.77×10^{-5} |

| Quantity | Value | Standard Uncertainty |
|------------------|--------------------------------|--------------------------------|
| $x(\text{HCHO})$ | $2.082 \mu\text{mol mol}^{-1}$ | $0.005 \mu\text{mol mol}^{-1}$ |

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Uncertainty calculations performed with Labview code

- $q_m(t)$ modelled by second order polynomial during analysis period
- q_v measured by Molbloc calibrated before measurements,
- $x_{\text{H}_2\text{O}}$ measured by CRDS calibrated by NPL, with/without permeation tube in chamber



Uncertainty of dynamic calibration gas

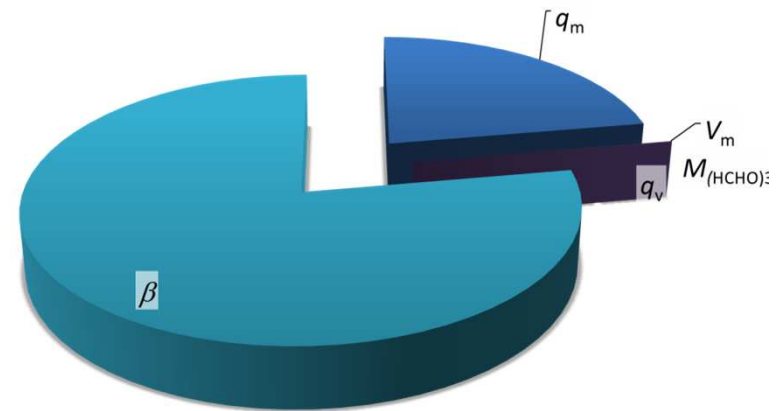
HCHO from trioxane

| Quantity | Value | unit | Standard relative uncertainty |
|-----------------------|---------|----------------------|-------------------------------|
| q_m | 6700.00 | ng min ⁻¹ | 9.1×10^{-4} |
| V_m | 22.4037 | L mol ⁻¹ | 1.52×10^{-5} |
| q_v | 2.5 | L min ⁻¹ | 5.12×10^{-4} |
| $M_{(\text{HCHO})_3}$ | 90.078 | g mol ⁻¹ | 2.22×10^{-5} |
| β | 1 | | 1.70×10^{-3} |

| Quantity | Value | Standard Uncertainty |
|------------------|--------------------------------|--------------------------------|
| $x(\text{HCHO})$ | $2.000 \mu\text{mol mol}^{-1}$ | $0.005 \mu\text{mol mol}^{-1}$ |

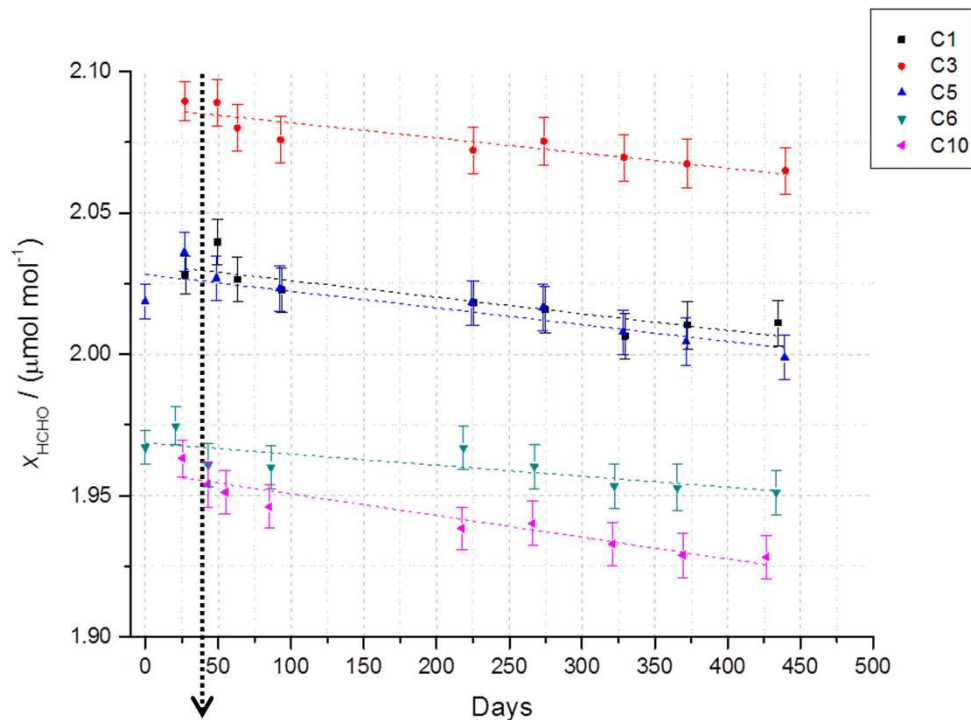
Uncertainty calculations performed with Labview code

- $q_m(t)$ modelled by second order polynomial during analysis period
- q_v measured by Molbloc calibrated before measurements,
- β measured by FTIR previously calibrated with trioxane, with/without trioxane-formaldehyde converter



Gas Standard Value Assignment and Stability Monitoring

HCHO mole fraction decrease



No impact of switching permeation source

Series of measurements

- With paraformaldehyde source first month
- With trioxane source after 30 days
- FTIR as main analytical instrument
- Model linear trend

x_0 fitted value at time 0

a_1 HCHO loss in $\mu\text{mol mol}^{-1} \text{ day}^{-1}$

t measurement time in days

$$x(t) = x_0 + a_1 t$$

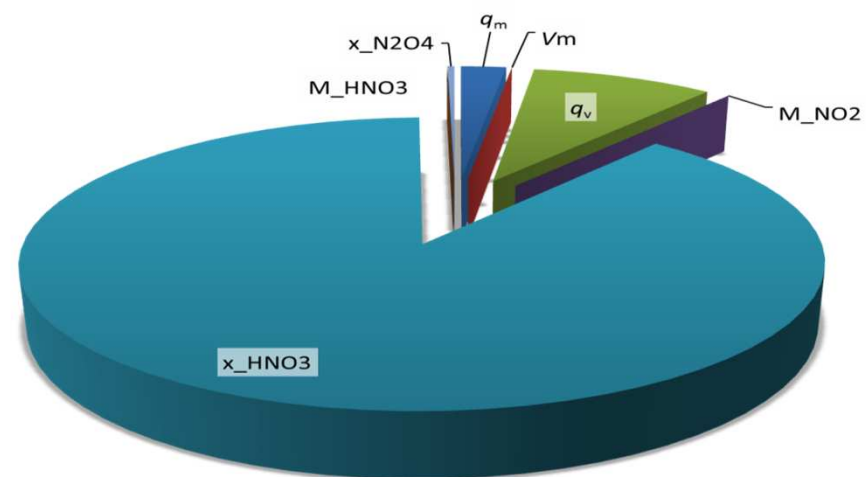
NO₂ standard value assignement with dynamic methods

| Quantity | Value | unit | Standard relative uncertainty |
|--------------|----------|------------------------|-------------------------------|
| q_m | 8357.30 | ng min ⁻¹ | 5.00×10^{-4} |
| V_m | 22.40037 | L mol ⁻¹ | 1.52×10^{-5} |
| q_v | 0.452 | L min ⁻¹ | 1.00×10^{-3} |
| M_{NO_2} | 46.0055 | g mol ⁻¹ | 3.04×10^{-5} |
| x_{HNO_3} | 104.00 | nmol mol ⁻¹ | 2.02×10^{-1} |
| M_{HNO_3} | 63.013 | g mol ⁻¹ | 1.86×10^{-5} |
| $x_{N_2O_4}$ | 0 | μmol mol ⁻¹ | 0.866 nmol/mol |

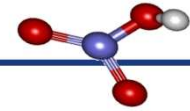
| Quantity | Value | Standard Uncertainty |
|-----------|-----------------------------|-----------------------------|
| $x(NO_2)$ | 8.86 μmol mol ⁻¹ | 0.03 μmol mol ⁻¹ |

HNO₃ quantification by FTIR
referenced to molecular parameters
(HITRAN)

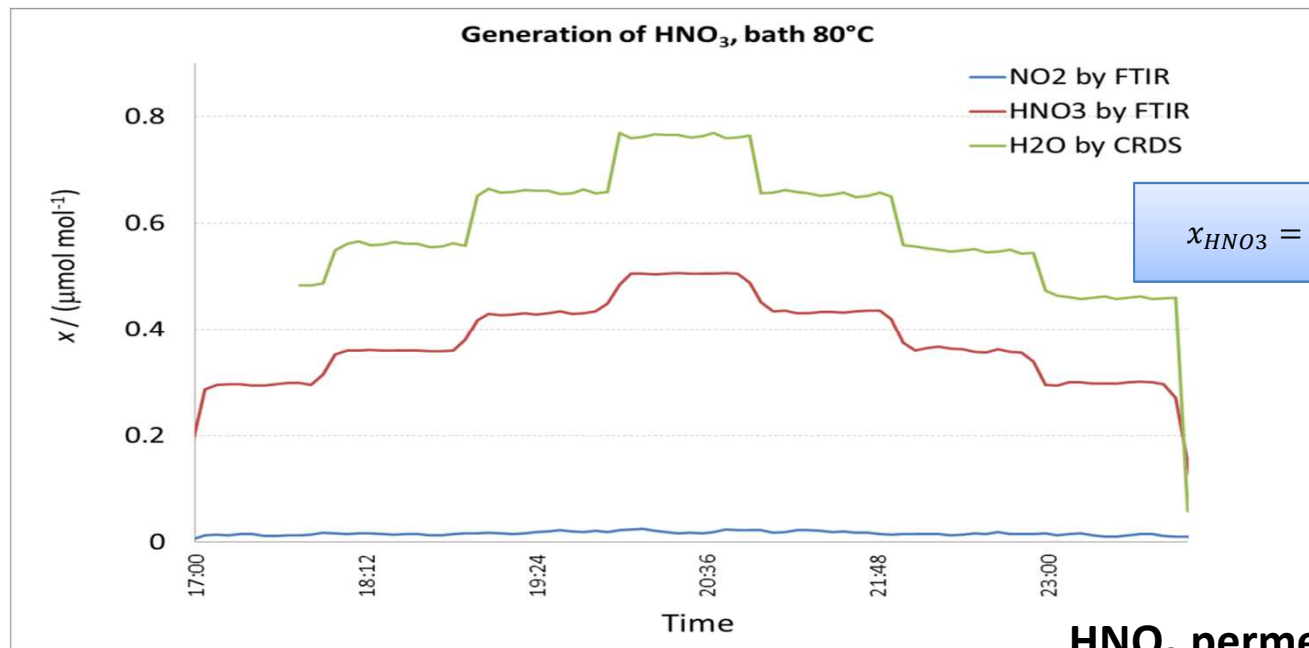
www.bipm.org



Reducing the uncertainty of HNO₃ measurements



Generation of dynamic mixtures of HNO₃ in nitrogen by permeation



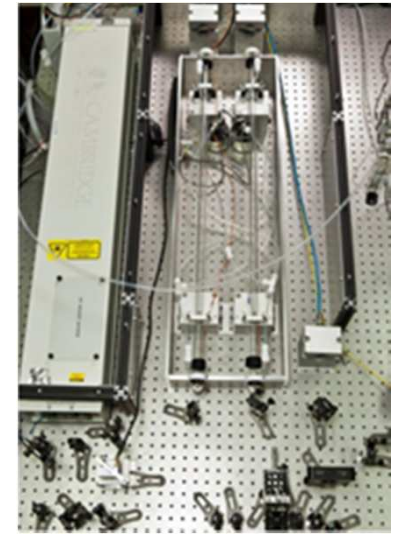
$$x_{HNO_3} = \frac{q_m V m}{q_v M_{HNO_3}} - \frac{M_{NO_2} x_{NO_2}}{M_{HNO_3}} - \frac{M_{H_2O} x_{H_2O}}{M_{HNO_3}}$$

HNO₃ permeation [200-500] nmol mol⁻¹

Permeation rate ~ 30 % H₂O

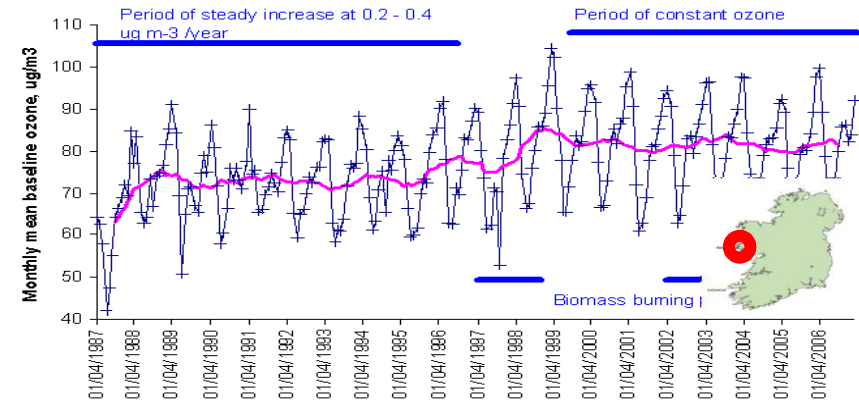
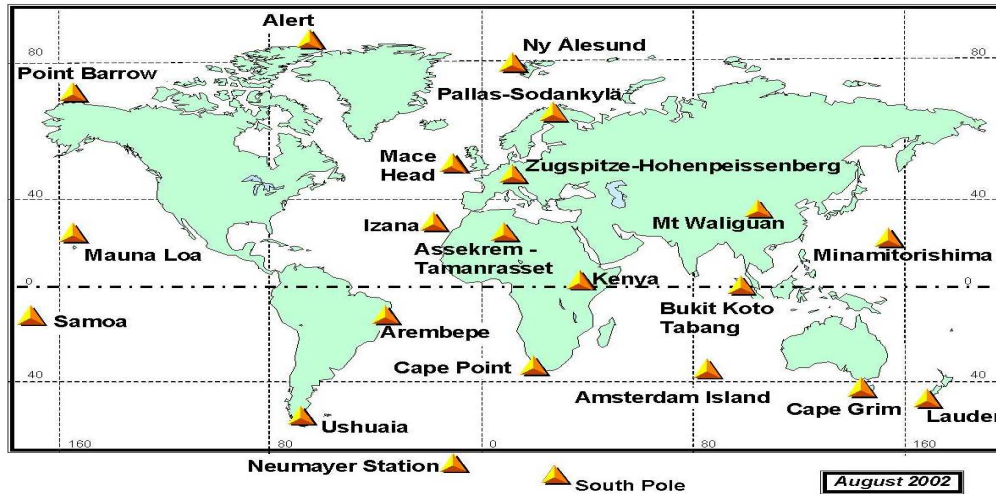
H₂O accurate quantification is crucial 37

Spectroscopic Methods

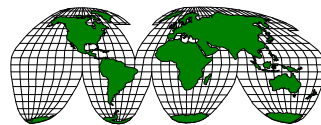


Surface Ozone Standards

WORLD METEOROLOGICAL ORGANIZATION
GLOBAL ATMOSPHERE WATCH GLOBAL NETWORK



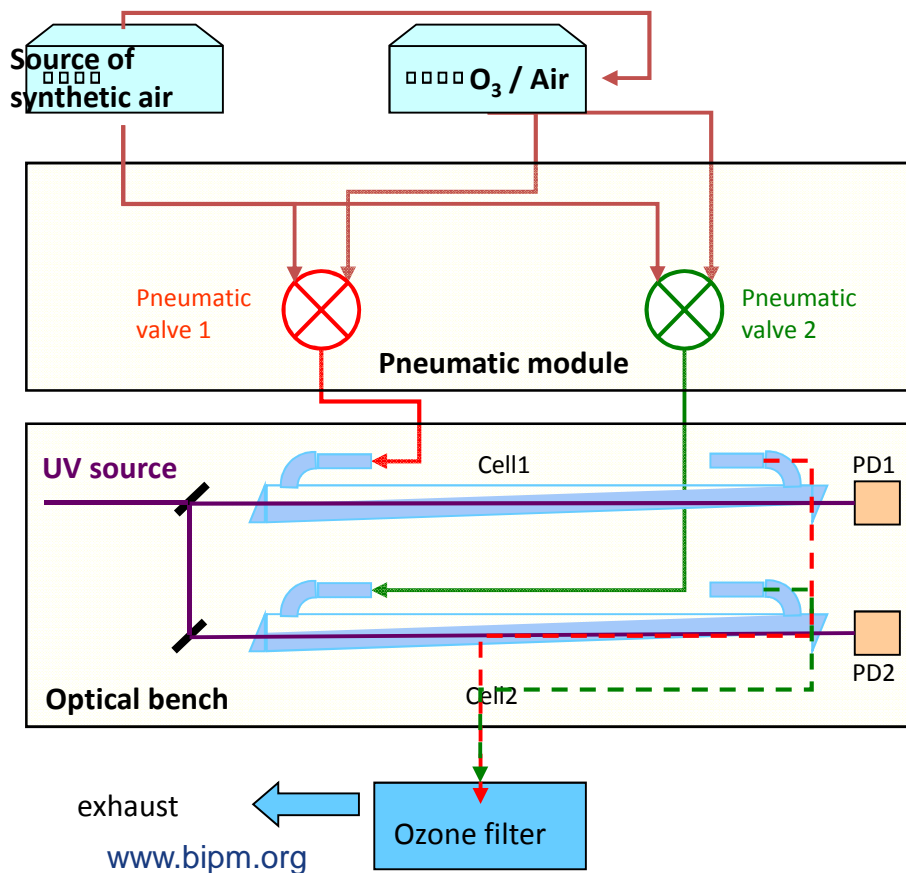
BIPM-NIST program to maintain the comparability of the worldwide network of ozone reference standards



NIST



Principle of an ozone photometer



- **Ozone generator** to produce ozone by photolysis of oxygen in the range 10 nmol mol⁻¹ to 1000 nmol mol⁻¹
- **Pneumatic module** to alternatively direct ozone/air gas flows in the two gas cells
- **Optical bench** with light source, optics, gas cells and detectors to perform absorption measurements

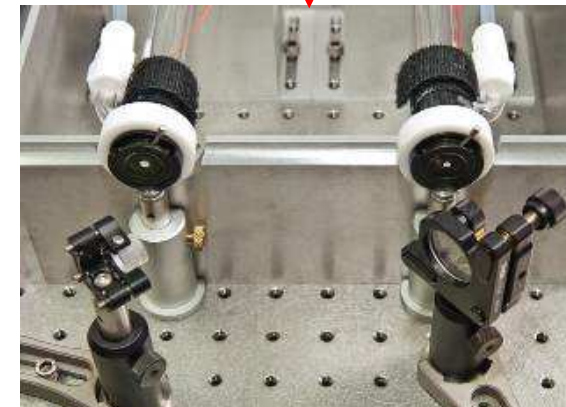
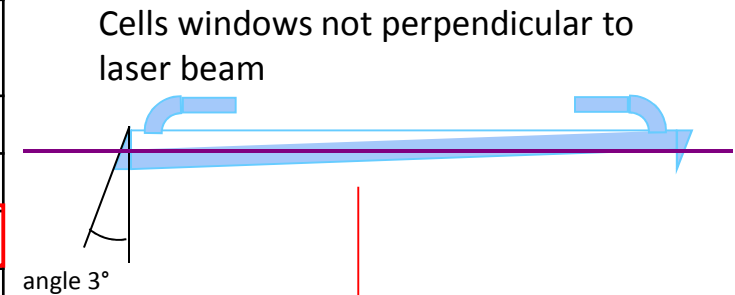
Measurement Equation:

$$x = \frac{-1}{2\alpha L_{\text{opt}}} \frac{T}{T_{\text{std}}} \frac{P_{\text{std}}}{P} \ln(D)$$

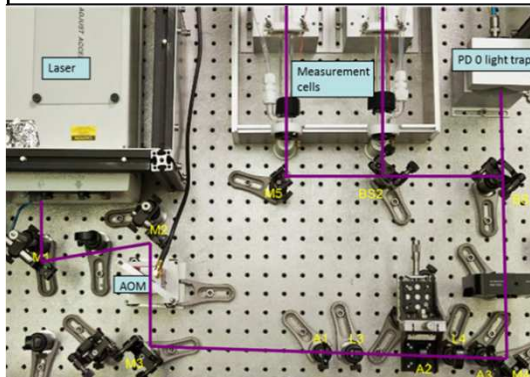
| | |
|---------------------------------|---|
| x / (nmol mol ⁻¹) | : ozone mole fraction in air |
| P / Pa | : Cell pressure |
| T / K | : Cell temperature |
| L_{opt} / m | : Light path length |
| D | : product of transmittances in both cells |
| α / cm ⁻¹ | : linear absorption coefficient |

Laser ozone photometer optical setup: Uncertainty budget

| Parameter | value | Standard uncertainty | Relative uncertainty |
|--|-----------|----------------------|----------------------|
| Temperature T | 295 K | 0.061 K | 2.1×10^{-4} |
| Pressure P | 1000 mbar | 0.64 mbar | 6.4×10^{-4} |
| Optical length L_{opt} | 893.9 mm | 0.4 mm | 4.5×10^{-4} |
| Product of transmittances D | 0.95 | 1.2×10^{-5} | 2.6×10^{-4} |
| Combined relative uncertainty (without the absorption cross-section) | | | 8.5×10^{-4} |

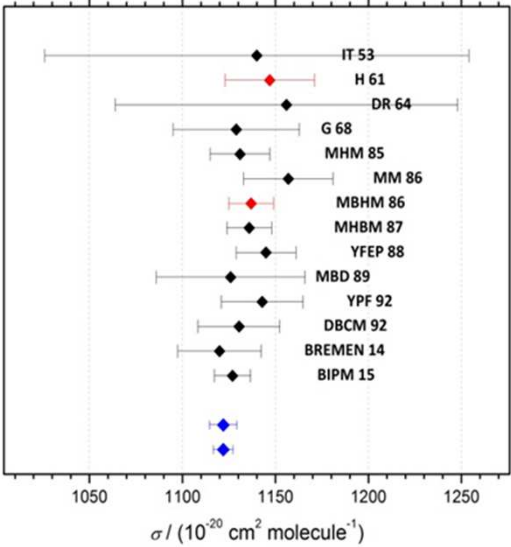


3 mm diaphragm before/after cells to help laser alignment



Major improvement compared to SRP = reduced uncertainty on the path length.

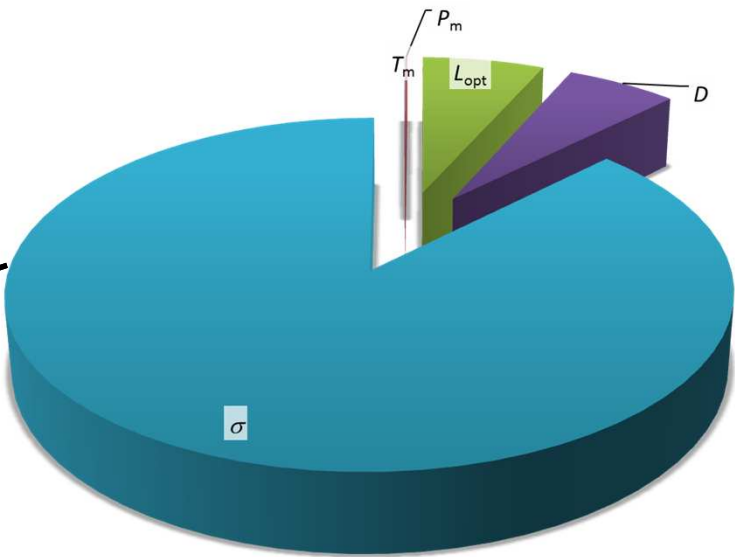
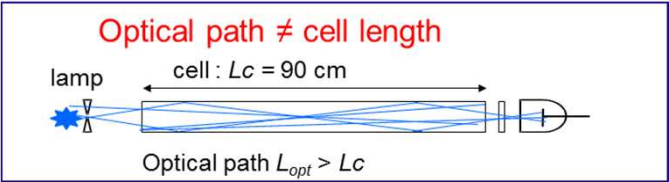
Uncertainty budget



- Inn and Tanaka 1953
- Hearn 1961
- DeMore and Raper 1964
- Griggs 1968
- Mauerbserger et al. 1985
- Molina and Molina 1986
- Mauerbserger et al. 1986
- Mauerbserger et al. 1987
- Yoshino et al. 1988
- Malicet et al. 1989
- Yoshino et al. 1992
- Daumont et al. 1992
- Gorshchev et al. 2014
- Viallon et al. 2015



Light path cell inside the gas cell



Absorption cross-section

- Fundamental property of the molecule
- Measured separately on known amount fractions
- Measured by ~ 15 groups
- Conventional value to be adopted

FTIR equipment and calibration strategies

FTIR hardware

Nexus spectrometer

Vertex 70v Vacuum FTIR (<1 hPa)

2- 0.7 L gas cells (Electropolished and Silcosteel)

1- 7 L gas cell (Silcosteel)

Software

MALT 4.4 (HITRAN)

MALT 5 (HITRAN)

P-MALT (MALT)

IMACC (Synthetic spectra or measured spectra)

E-TRANS (HITRAN)



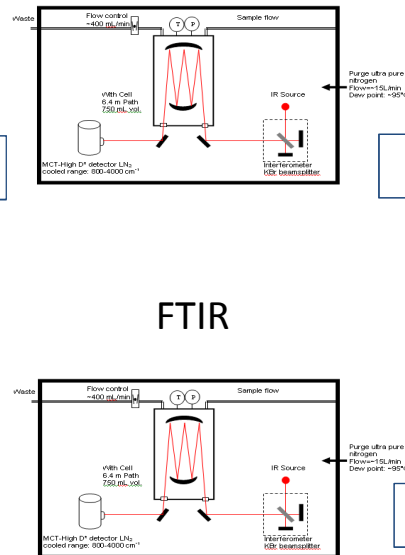
Using FTIR **with** and without calibration standards

BIPM NO₂ Facility



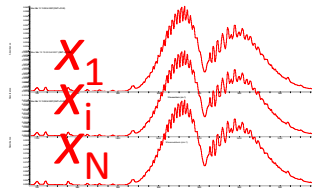
u_{xNO_2}

FTIR



u_{stab}

Set of spectra



Uncertainties

Least-square fit

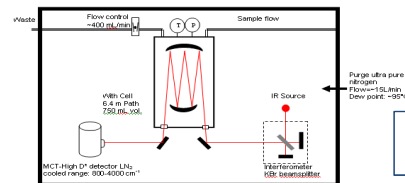


$x = !!$
 $u(x) = !!$

Unknown

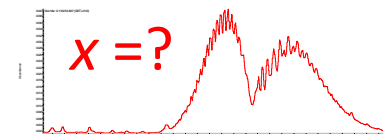


FTIR

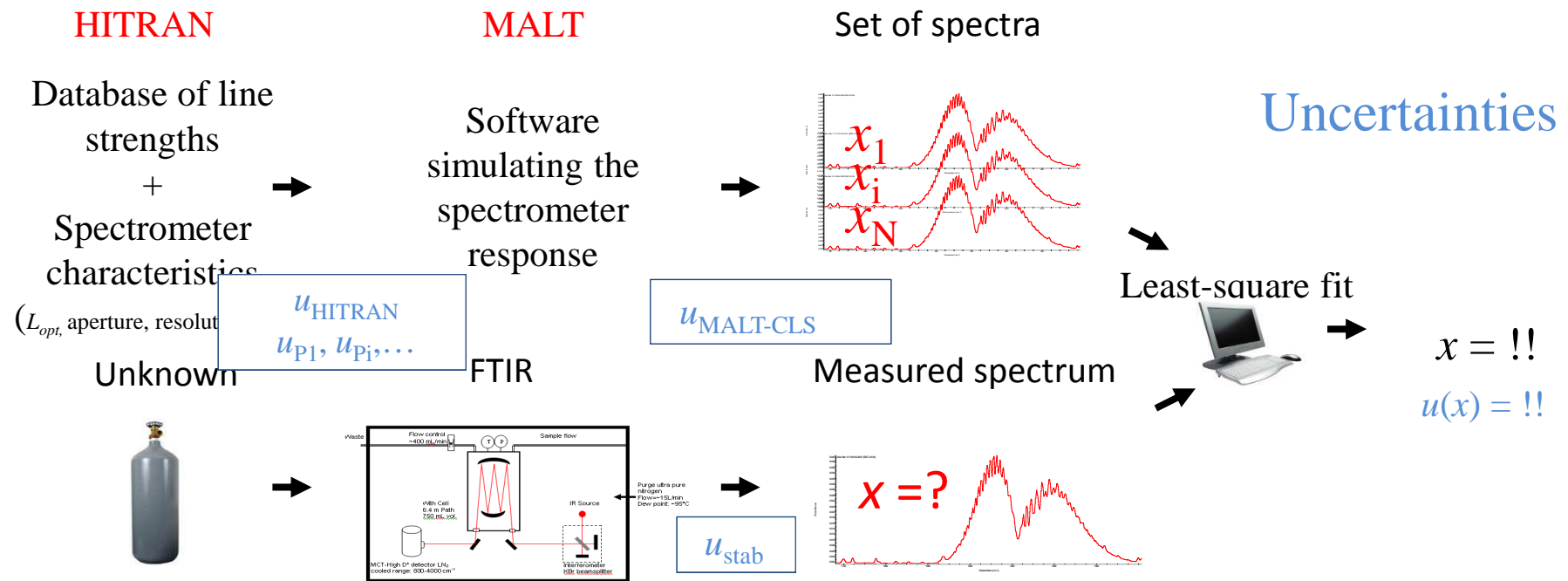


u_{stab}

Measured spectrum



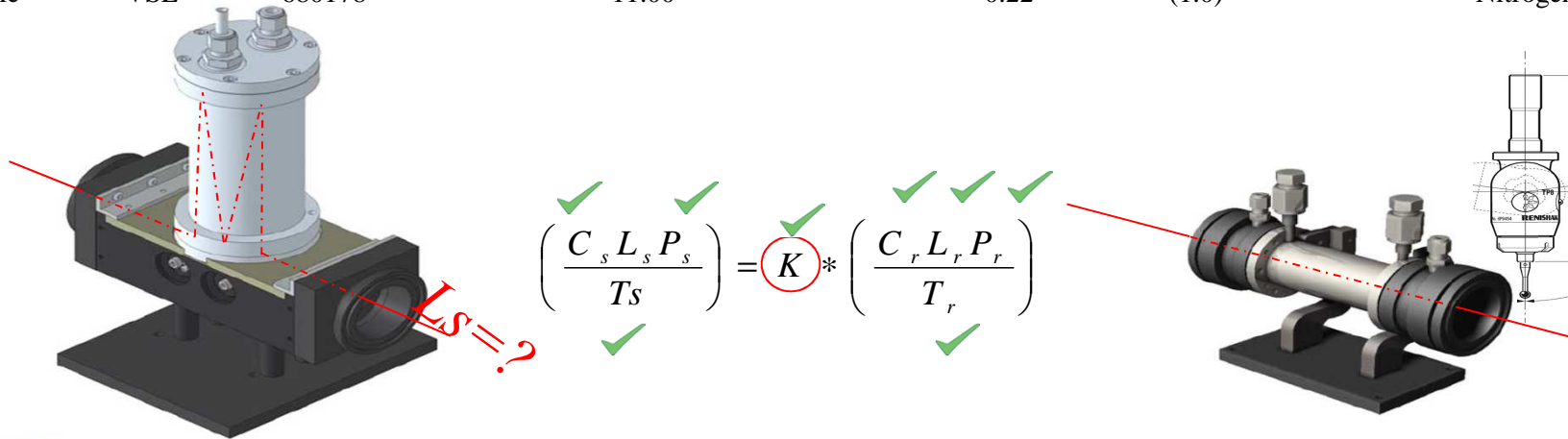
Using FTIR with and without calibration standards



Pathlength uncertainty L_{opt}

Determination of the White-cell's path length

| Use | Origin | #Cylinder | Assigned NO ₂ mole fraction μmol·mol ⁻¹ | Certified standard uncertainty μmol·mol ⁻¹ (%) | Matrix gas |
|-----------|--------|-----------|--|--|-----------------|
| Reference | NPL | L1000025 | 99.99 | 0.8 (0.8) | Nitrogen/Oxygen |
| Sample | VSL | 680178 | 11.00 | 0.22 (1.0) | Nitrogen |



Uncertainty of applying spectral fitting ... (MALT)

| MALT input parameter | Estimated value x_i | Unit | Assumed distribution | Standard uncertainty $u(x_i)$ | Measurand variation DY | Index to uncertainty DY/2 | Index to uncertainty in % |
|--------------------------------|--------------------------|------------------|----------------------|----------------------------------|---------------------------|------------------------------|------------------------------|
| Pathlength | 6.45 | m | normal | 0.085 | -0.258 | -0.13 | 61.04 |
| Temp | 27.7 | °C | normal | 1.37 | 0.175 | 0.09 | 28.08 |
| Amount | 10 | µmol/mol | rectangular | 1 | -0.075 | -0.04 | 5.16 |
| % halfwidths for Voigt | 50 | cm ⁻¹ | rectangular | 20 | -0.059 | -0.03 | 3.19 |
| Resolution | 0.964 | cm ⁻¹ | rectangular | 0.062 | 0.052 | 0.03 | 2.48 |
| Colimator appertures | 4.666 | mm | rectangular | 0.1 | -0.005 | 0 | 0.02 |
| Presure | 794 | Torr | normal | 0.159 | 0.004 | 0 | 0.01 |
| Region <1600 cm-1 | 1660 | cm ⁻¹ | | 0 | | 0 | 0 |
| Region >1600cm-1 | 1550 | cm ⁻¹ | | 0 | | 0 | 0 |
| % halfwidths | 5 | % | rectangular | 3 | 0 | 0 | 0 |
| Colimator focal length | 152 | mm | rectangular | 1 | 0 | 0 | 0 |
| SYm1 | 0 | - | rectangular | 0.1 | 0.001 | 0 | 0 |
| SYm2 | 0 | - | rectangular | 0.1 | 0.0023 | 0 | 0 |
| Wavenumber shift rel to Hitran | 0 | cm ⁻¹ | rectangular | 0.1 | 0 | 0 | 0 |
| Base line offset | 0 | cm ⁻¹ | rectangular | 0.3 | 0 | 0 | 0 |

NO₂ mole fraction $x = 11.08 \mu\text{mol/mol}$

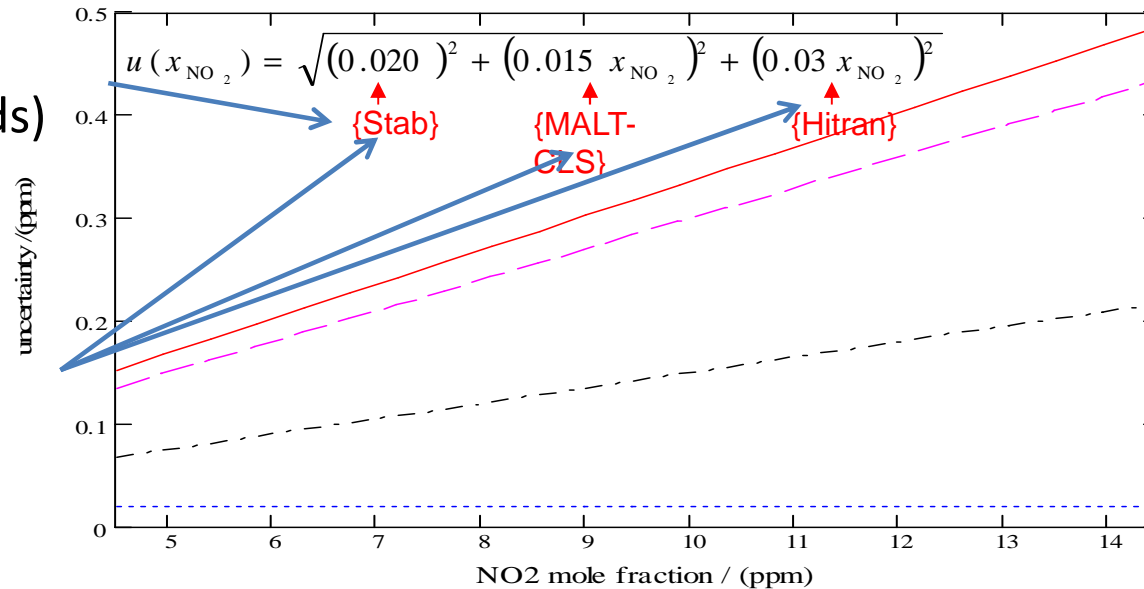
combined uncertainty $u(x) = 0.165 \mu\text{mol/mol}$

$u_R(x) = 1.50\%$

Total uncertainty:

Mode A
(With standards)

Mode B
(Without standards)

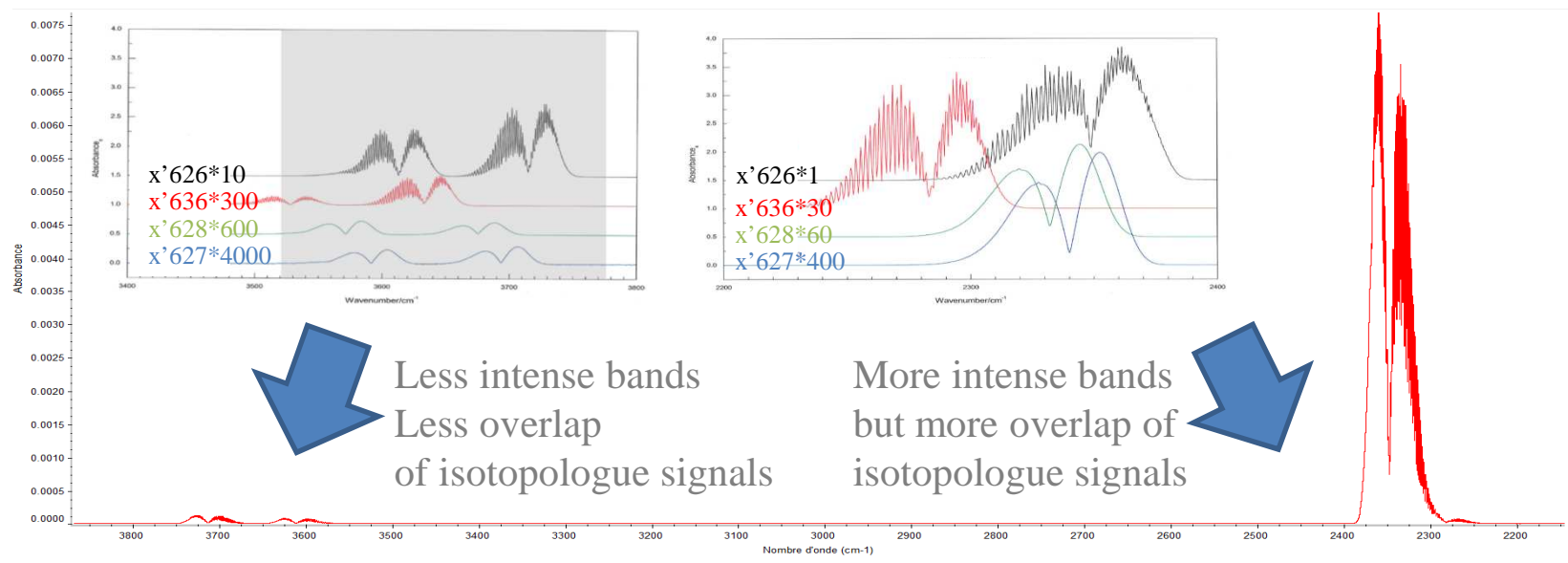


Numerical equation in $\mu\text{mol mol}^{-1}$

- combined uncertainty
- ⋯ stability
- - hitran
- - MALT-CLS

$x_{NO_2} = 10 \mu\text{mol mol}^{-1}$

Measurement of CO₂ (and CO₂ isotopologues) by FTIR



Accurate measurement of CO₂ (and CO₂ isotopologues) by FTIR

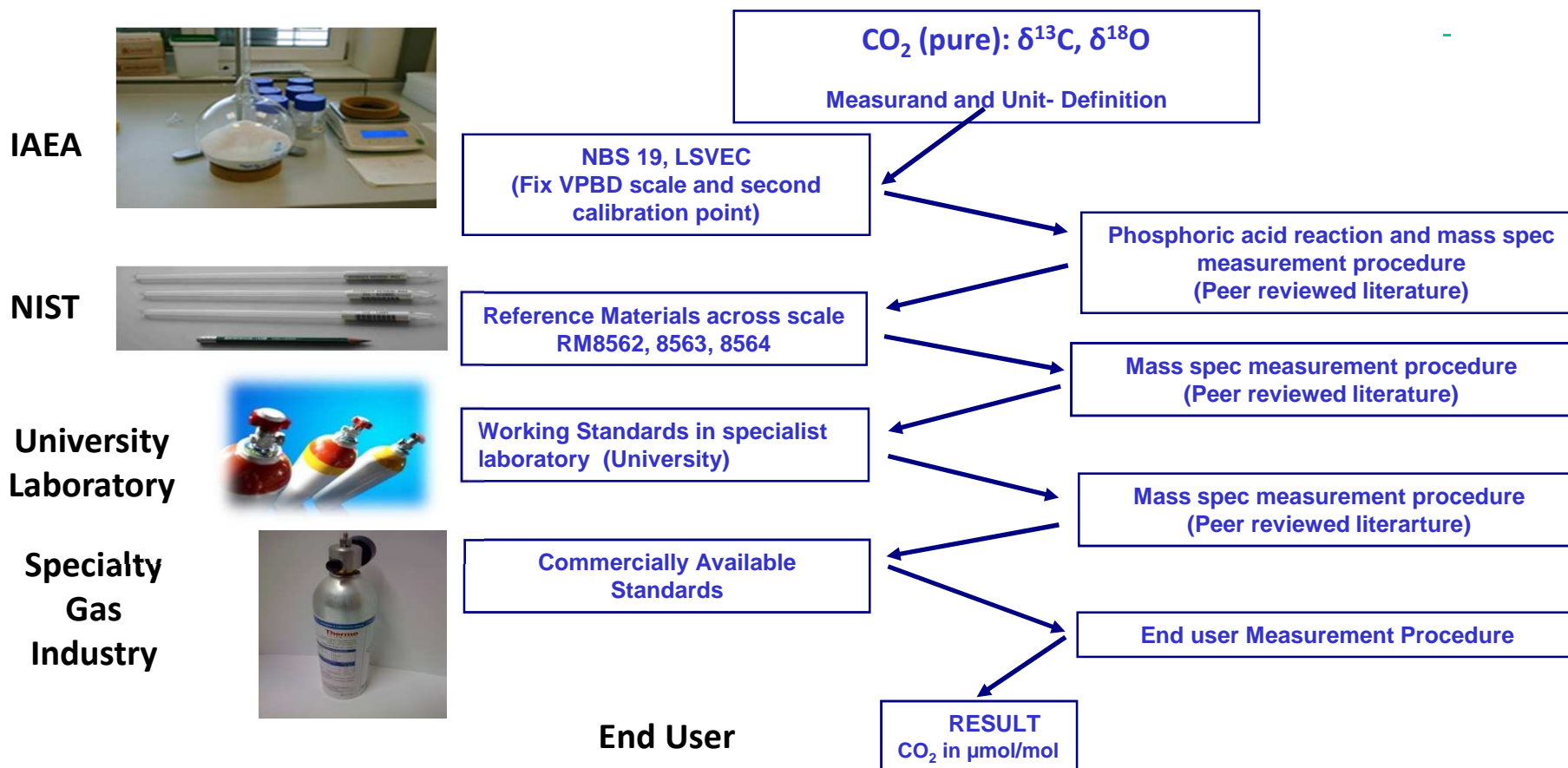
| M/z | CO ₂ Isotope |
|-----|--|
| 44 | ¹² C ¹⁶ O ₂ |
| 45 | ¹³ C ¹⁶ O ₂ , ¹² C ¹⁶ O ¹⁷ O |
| 46 | ¹² C ¹⁶ O ¹⁸ O, ¹³ C ¹⁶ O ¹⁷ O, ¹² C ¹⁷ O ₂ |
| 47 | ¹³ C ¹⁶ O ¹⁸ O, ¹² C ¹⁷ O ¹⁸ O, ¹³ C ¹⁷ O ₂ |
| 48 | ¹³ C ¹⁷ O ¹⁸ O, ¹² C ¹⁸ O ₂ |
| 49 | ¹³ C ¹⁸ O ₂ |



Isotope ratio: $\frac{^{13}\text{C}}{^{12}\text{C}}$

$$\delta^{13}\text{C} = \frac{\frac{^{13}\text{C}}{^{12}\text{C}}(\text{sample}) - \frac{^{13}\text{C}}{^{12}\text{C}}(\text{standard})}{\frac{^{13}\text{C}}{^{12}\text{C}}(\text{standard})}$$

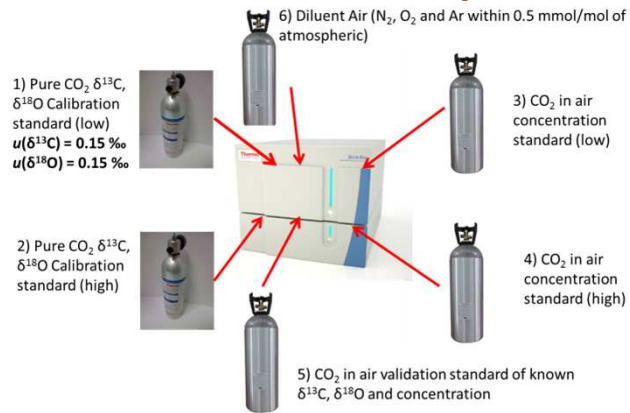
Traceability Chain for δ -scale CO₂ isotope ratio measurements



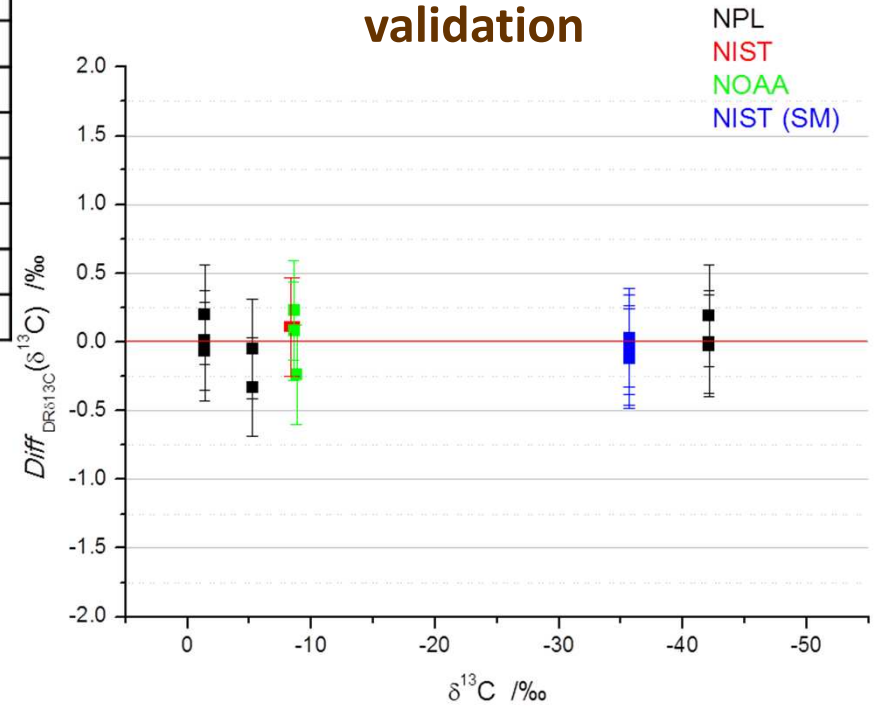
Measuring Carbon isotope ratios in CO₂ in Air

| Quantity | Analytical Method | Range | Analytical Standard Uncertainty |
|--------------------------------------|-------------------|---------------------------|---------------------------------|
| X _{CO2} | FTIR | (300 to 850) μmol/mol | 0.03 μmol/mol |
| X _{CO2} | IRIS | (300 to 850) μmol/mol | 0.04 μmol/mol |
| X _{CO2} | GC | (300 to 850) μmol/mol | 0.04 μmol/mol |
| X _{CO2} | PVT system | (300 to 850) μmol/mol | 0.1 μmol/mol |
| δ ¹³ C (CO ₂) | IRIS | (-1 to -42)‰ (VPDB scale) | 0.2 ‰ |
| δ ¹⁸ O (CO ₂) | IRIS | (-1 to -34)‰ (VPDB scale) | 0.4 ‰ |
| δ ¹³ C (CO ₂) | FTIR | (-1 to -42)‰ (VPDB scale) | 0.4 ‰ |
| δ ¹⁸ O (CO ₂) | FTIR | (-1 to -34)‰ (VPDB scale) | 3.0 ‰ |

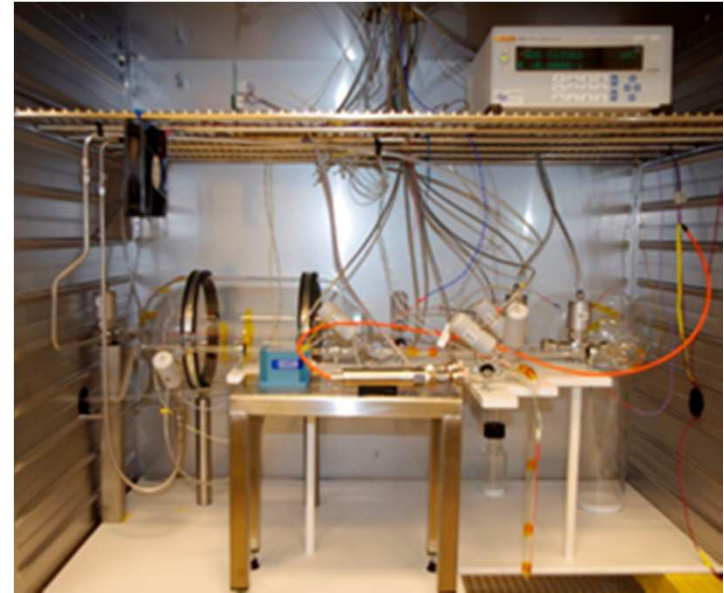
IRIS Calibration Sequence



δ¹³C CO₂ measurement validation

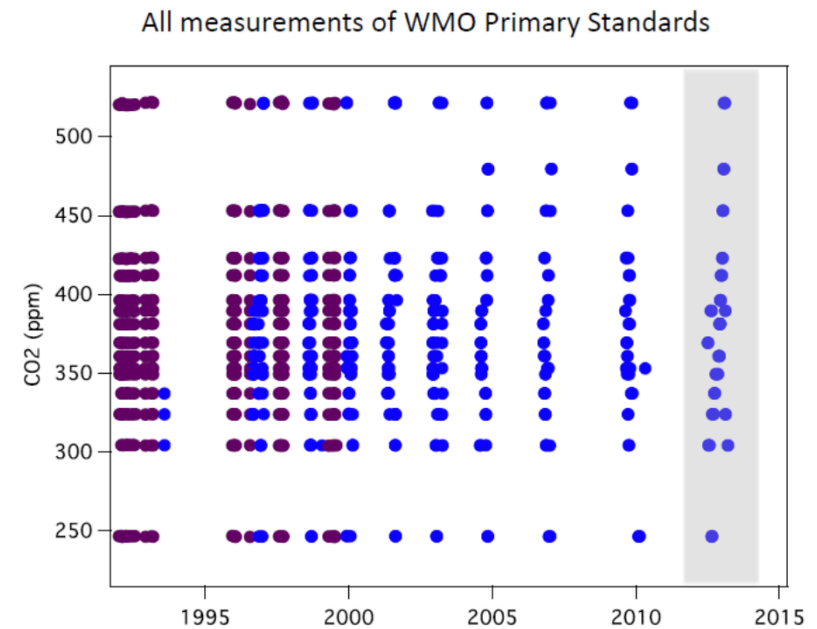
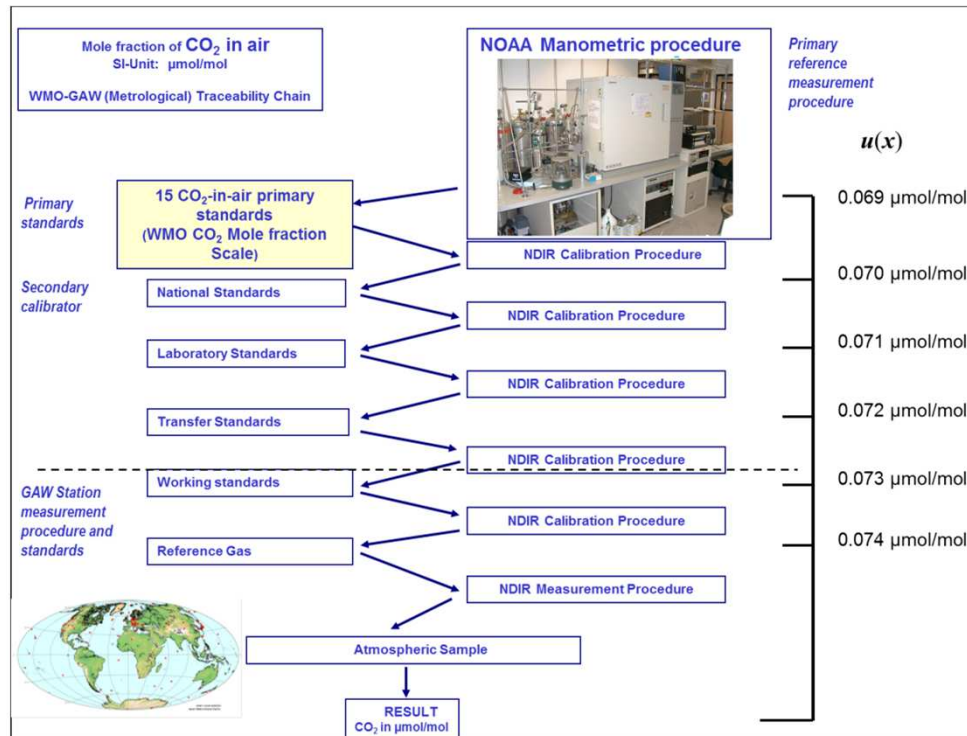


Manometric Methods



WMO GAW network is the designated baseline network for CO₂ and CH₄

- NOAA/ESRL is the Central Calibration Laboratory for CO₂ and CH₄ (and other trace gases)



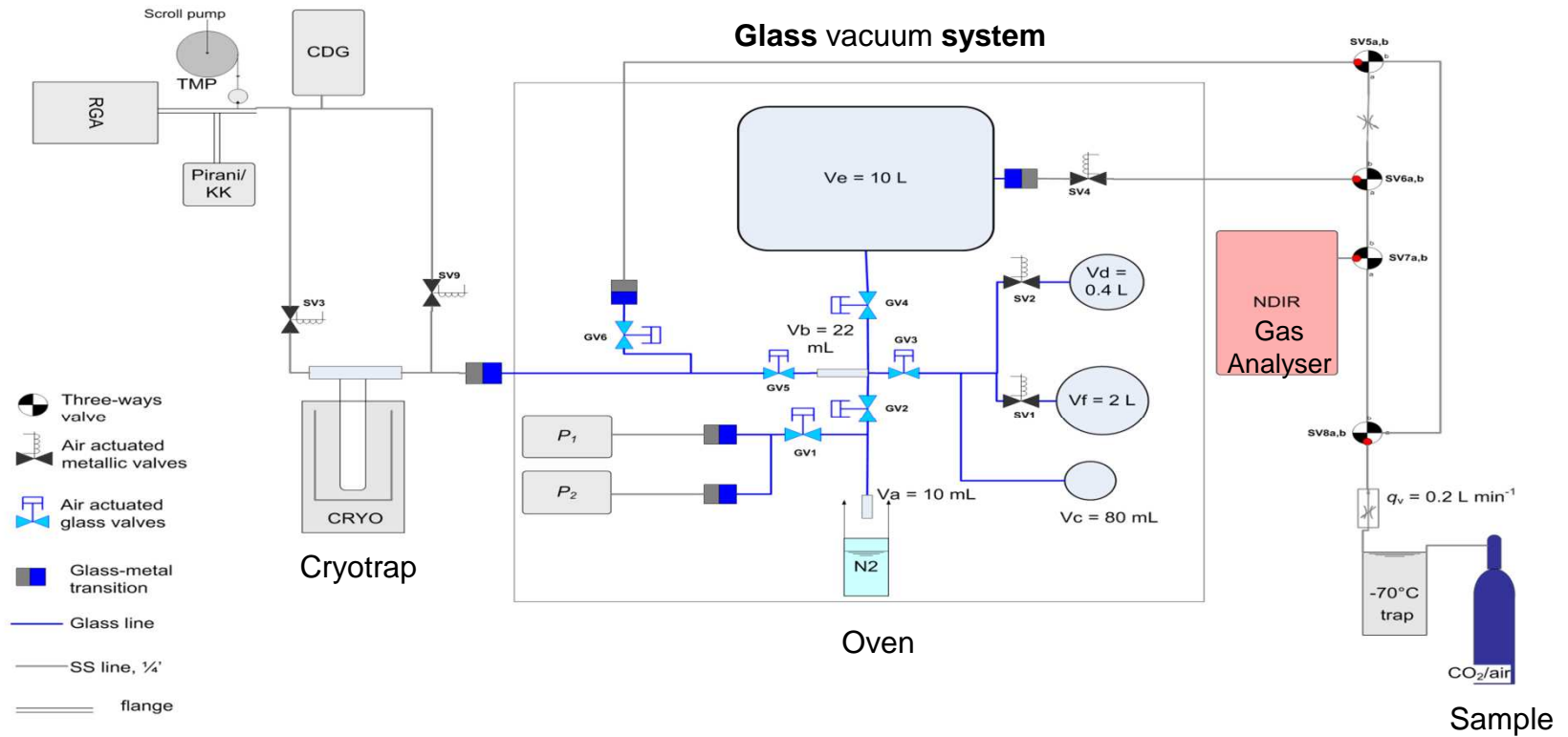
Manometry: Basic principle

- ◆ Initially well known amount of air, V_{air} , T_{air} and P_{air}
- ◆ Extract CO_2 from the air by cooling
- ◆ Expand the CO_2 in another (smaller) well known volume, V_{CO_2} , T_{CO_2} and P_{CO_2}

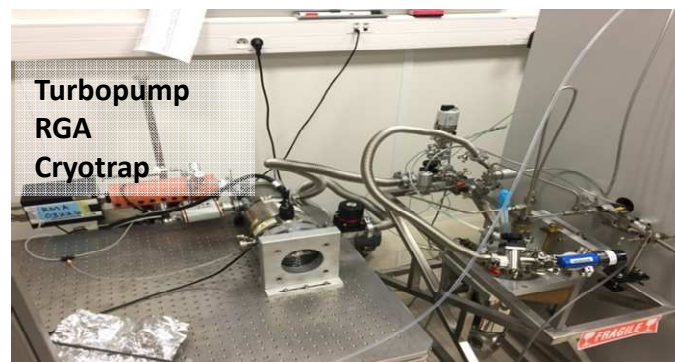
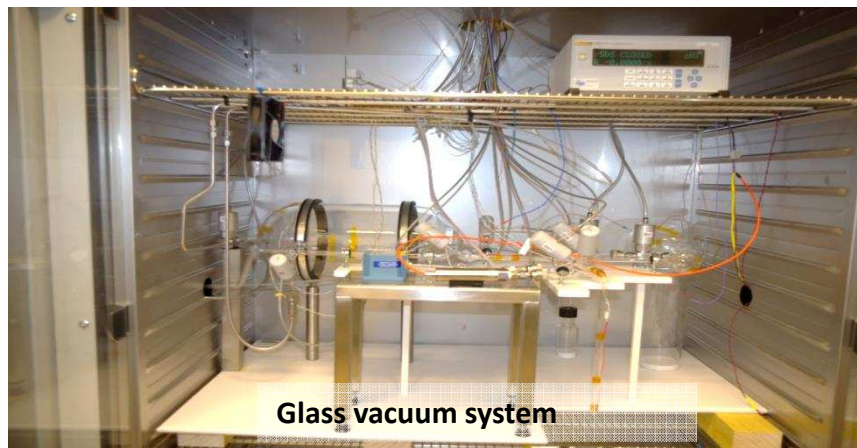
$$x_{CO_2} = \frac{n_{CO_2}}{n_{air}} = \frac{1}{R_V} \frac{P_{CO_2}}{P_{air}} \frac{T_{air}}{T_{CO_2}} \frac{1 + \frac{B_{air}(T_{air})P_{air}}{RT_{air}}}{1 + \frac{B_{CO_2}(T_{CO_2})P_{CO_2}}{RT_{CO_2}}}$$

$$R_V = \frac{V_{air}}{V_{CO_2}}$$

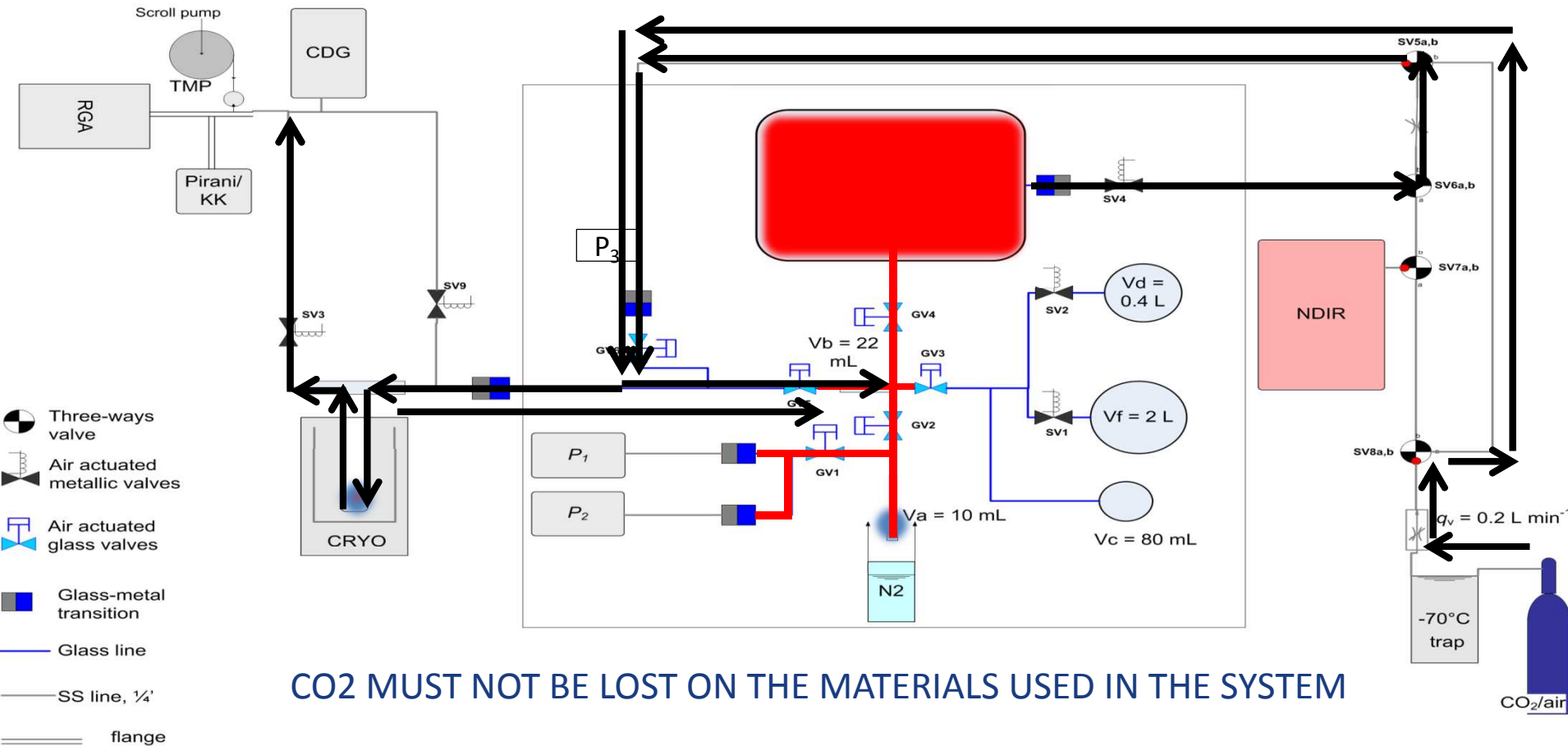
System layout: CO₂ Manometry



System overview



Principle of operation



CO₂ MUST NOT BE LOST ON THE MATERIALS USED IN THE SYSTEM

Cold trapping

When **trapping**, should be:

- Hot enough to allow N_2 , O_2 , Ar, CH_4 , N_2O to pass
- Cold enough to capture H_2O , and CO_2

When **distilling**, should be:

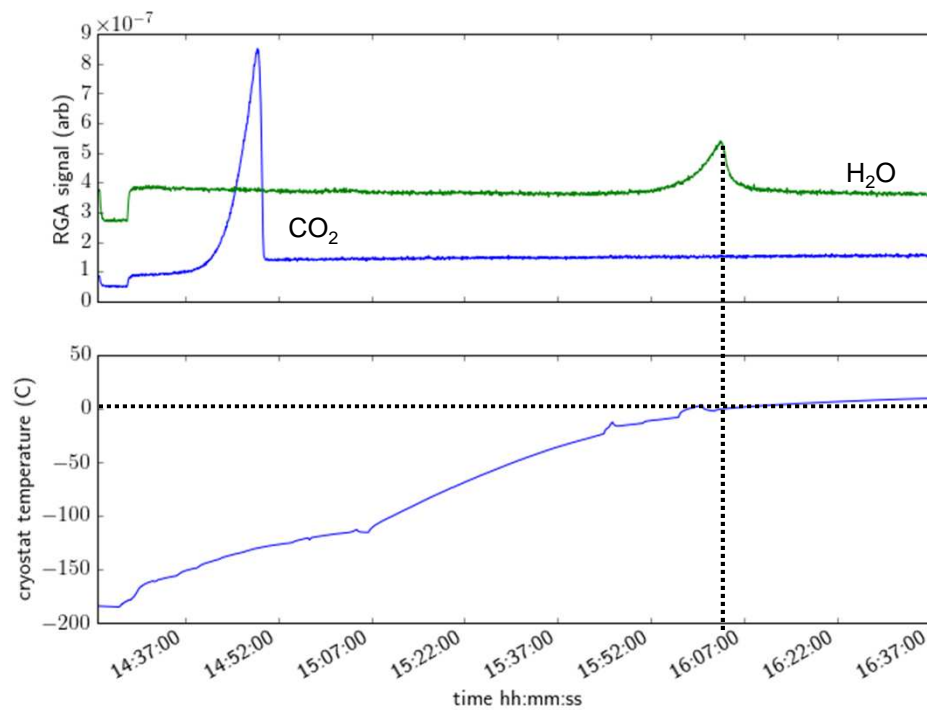
- Cold enough to keep H_2O ,
- Hot enough to release CO_2

Needs to be:

- **Long enough** to make sure CO_2 is fully captured (two mechanisms...possible issues)
- Made of materials that don't cause chemical reactions

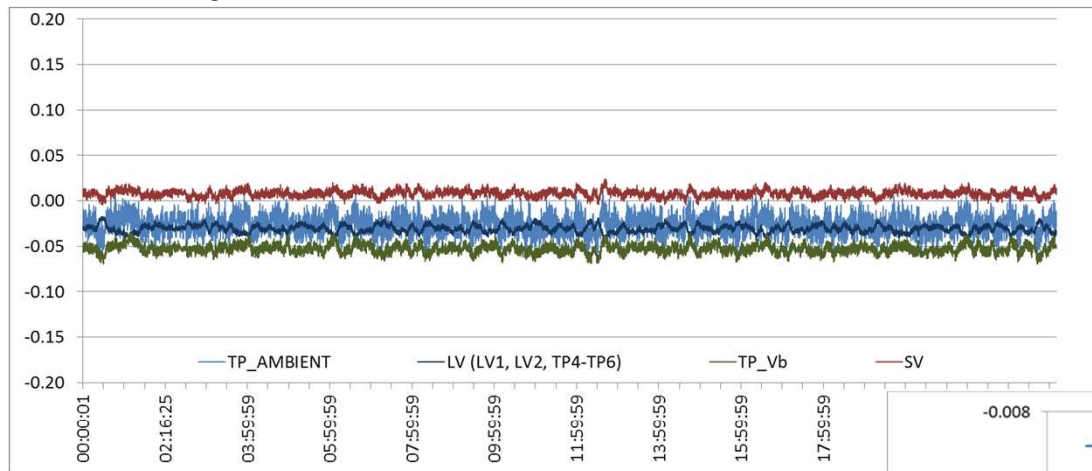


RGA can diagnose input cold trap



Temperature and Pressure Measurement

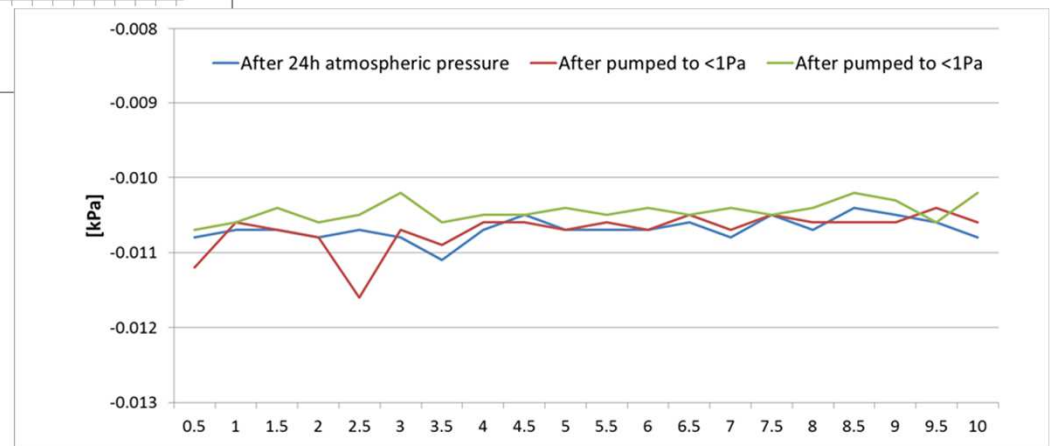
◆ Temperature: Differences below 0.05°C



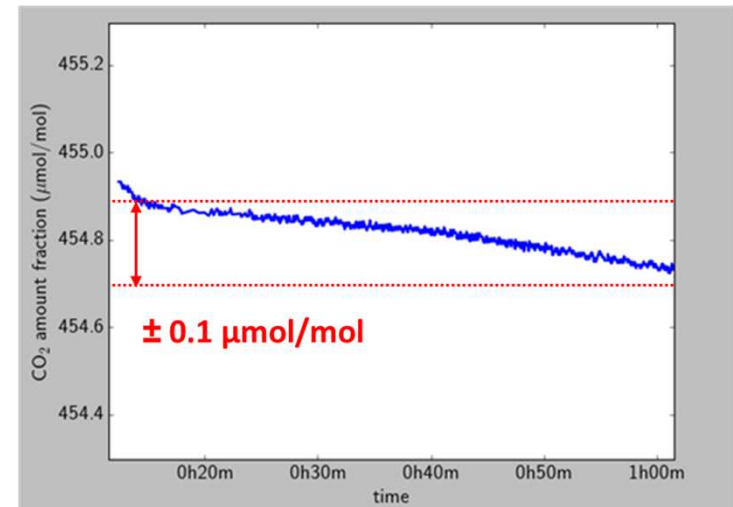
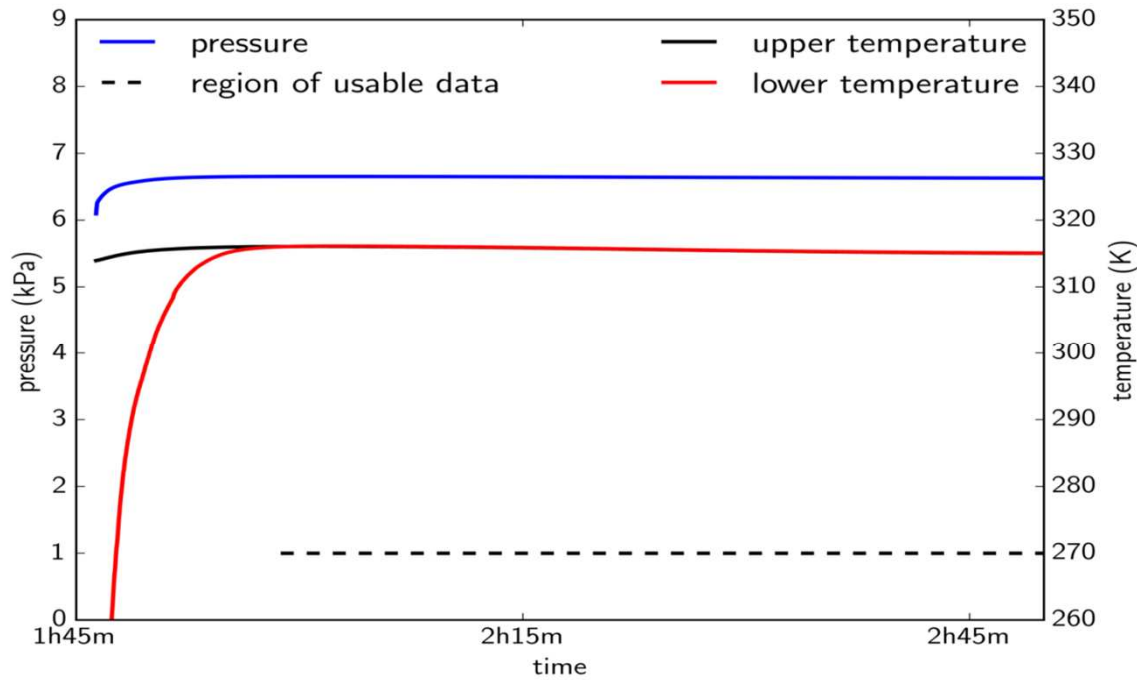
Comparison against external reference standard kept at 100 kPa.

Short term stability and hysteresis are excellent, well below 1 Pa.

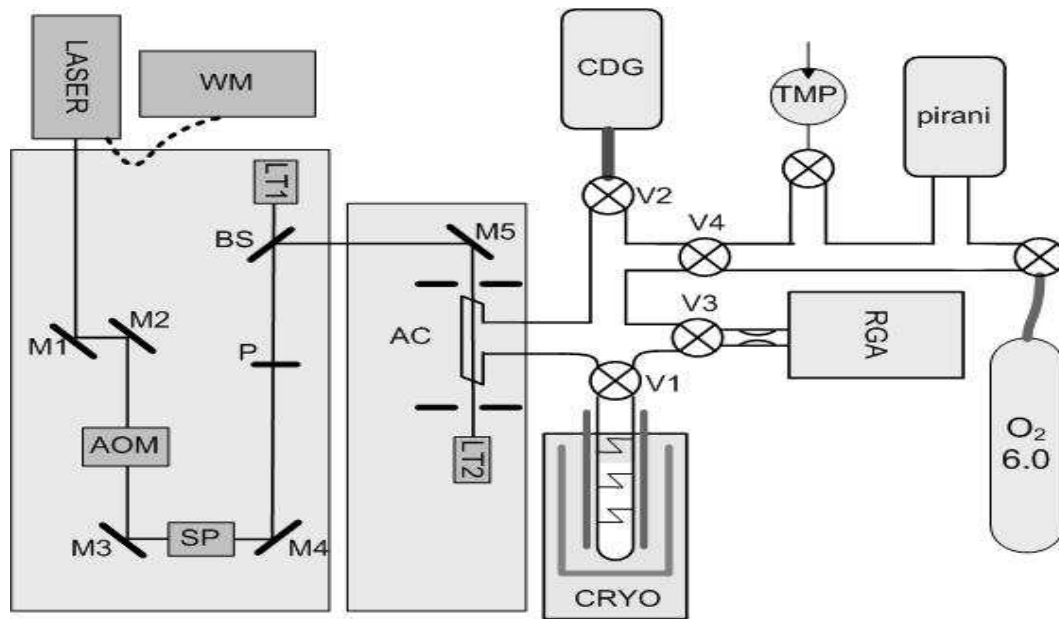
Pressure Measurement at two distinct levels, 100 kPa and 30 kPa.



CO₂ Extraction sequence

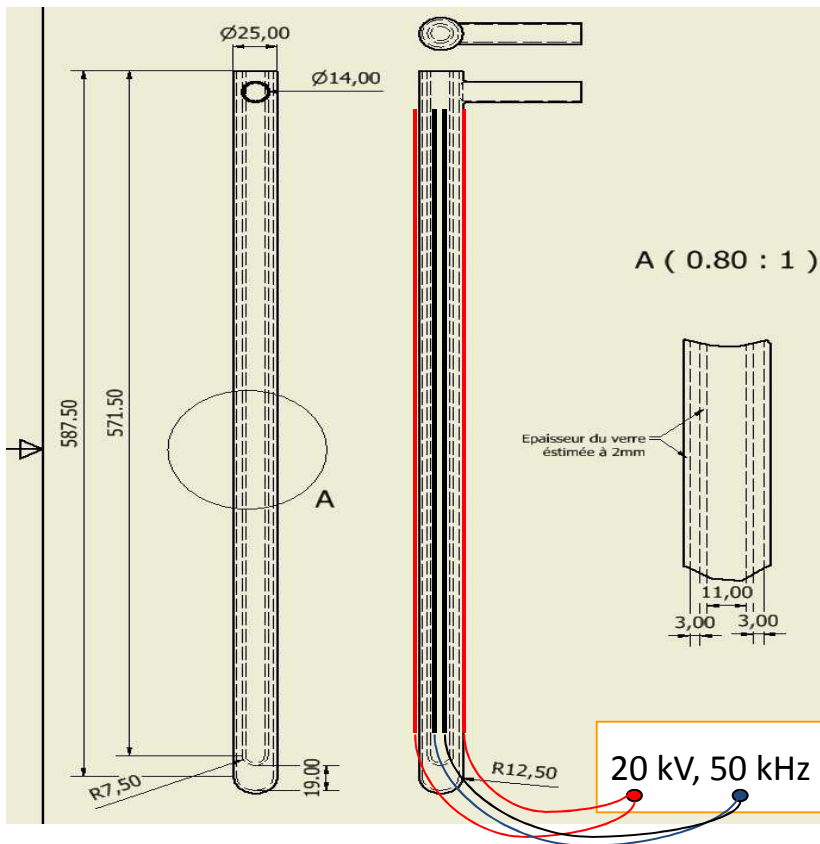


Manometric System for O₃ Cross Section Measurements

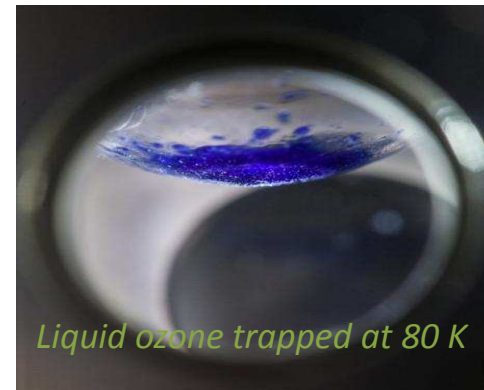


- AOM Accousto-Optic Modulator;
- BS Beam Splitter;
- CDG Capacitive Diaphragm Gauge (Baratron);
- CRYO Cryogenic ozone generator;
- LT Light Trap;
- M Mirror;
- RGA Residual Gas Analyser ;
- TMP Turbo Molecular Pump;
- V Valve;
- WM Wavemeter

Ozone generator

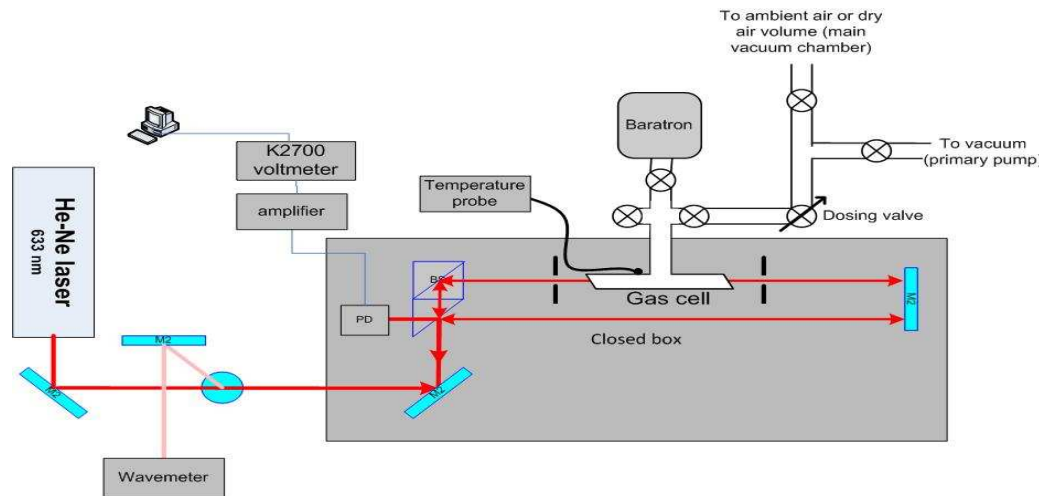


- ⊕ Ozone produced by discharges in pure oxygen
- ⊕ generator = double wall cylinder in glass
- ⊕ generation part inserted in cryostat
- ⊕ controllable cryostat temperature from 74 K and above



Absorption path length measurements by interferometry

Michelson interferometer to deduce L_{opt} in the cell in which the pressure is varied



Pressure in the cell: 1 bar \rightarrow 0.1 mbar

$\rightarrow F$ fringes on the photodiode

\rightarrow Path length L_0

$$(n - 1) L_0 = F \frac{\lambda_a}{2}$$

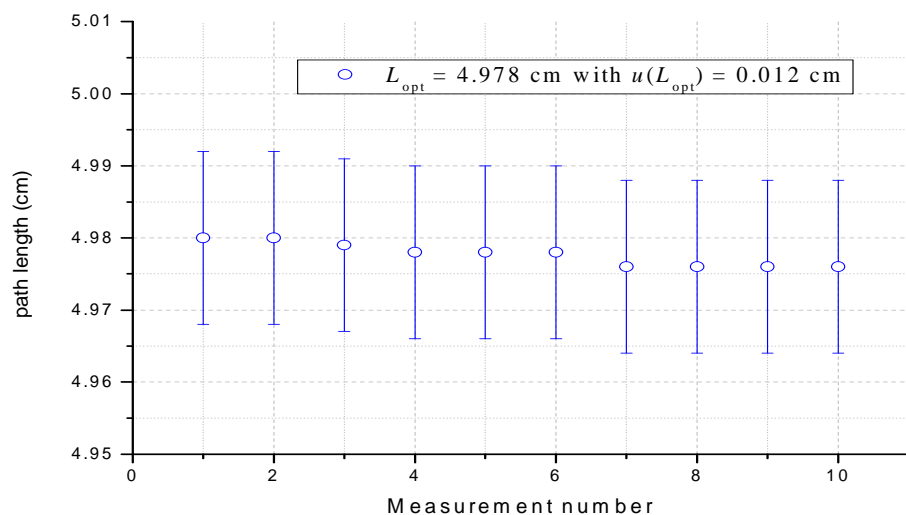
- n : index of refraction of air
- L_0 / m : light path length
- F : number of fringes
- λ_a / m : laser wavelength

Edlen formula for the air index of refraction at pressure P and temperature T

$$n - 1 = \frac{p \cdot 10^{-8} \left[8342.54 + 2406147(130 - \sigma^2)^{-1} + 15998(38.9 - \sigma^2)^{-1} \right] \left[1 + 10^{-8} \cdot (0.601 - 0.00972T) p \right]}{96095.43 (1 + 0.003661T)}$$

Absorption path length measurements by interferometry

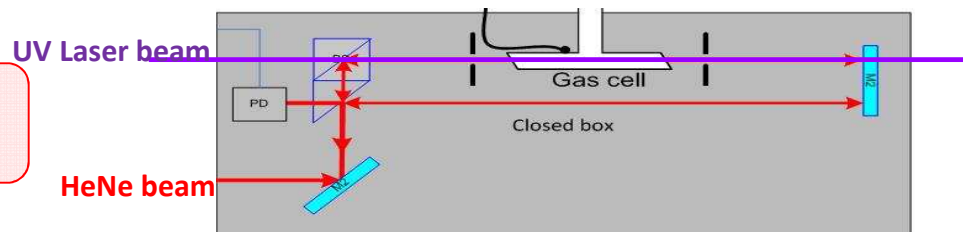
Measurements



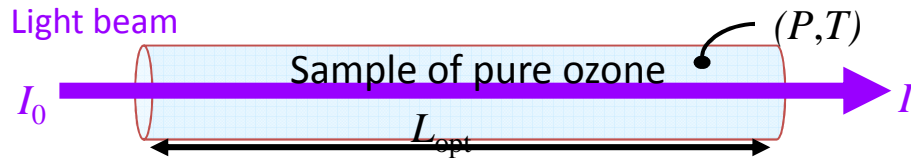
Uncertainty budget

| Quantity | Value | Standard Uncertainty |
|------------------|------------------------|-----------------------------------|
| F | 42 | 0.102 |
| T | 22.3 °C | 0.018 °C |
| P_a | 1003.25 hPa | 0.852 Pa |
| λ_a | 0.632823 μm | $3.47 \times 10^{-6} \mu\text{m}$ |
| λ_v | 0.632991 μm | $0.29 \times 10^{-6} \mu\text{m}$ |
| L_{opt} | 4.979 cm | 0.012 cm |

OK to be used for cross-section measurements, provided same laser path in the gas cell



Ozone cross-section measurement principle



$$\sigma_{O_3} = \frac{1}{L_{opt}} \frac{T}{P_{O_3}} \frac{R}{Na} \ln\left(\frac{I}{I_0}\right)$$

Pressure : pressure sensors measure **total pressure** P_T , not partial pressure $P_{O_3} = x(O_3) P_T$

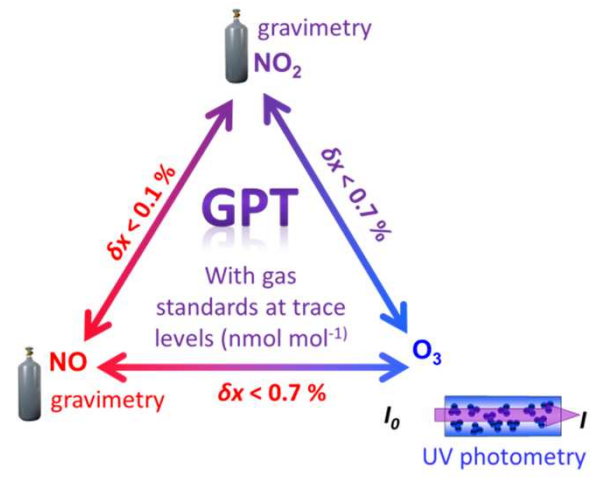
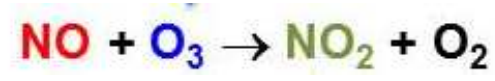
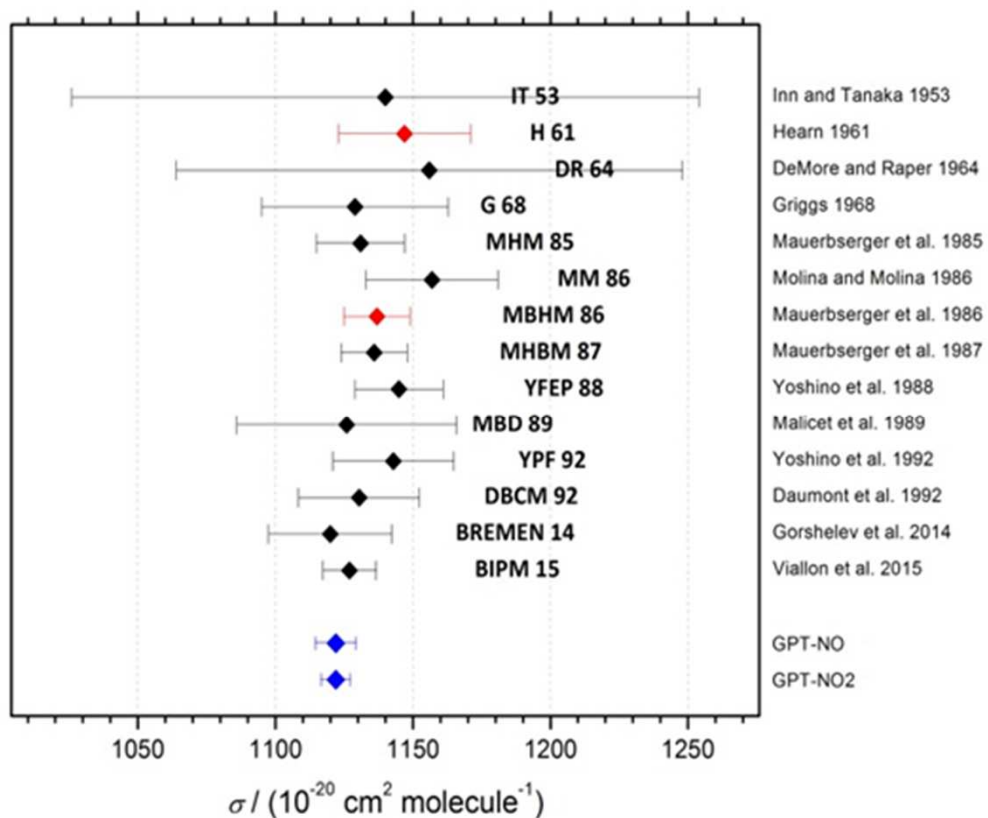
$$\sigma_{O_3} = \frac{1}{L_{opt}} \frac{T}{P_T \cdot x(O_3)} \frac{R}{Na} \ln\left(\frac{I}{I_0}\right)$$

Purity = assessment of impurities

- condensables x_C
- non-condensables x_{NC}

$$\sigma_{O_3} = \frac{1}{L_{opt}} \frac{T}{P_T \cdot \left[1 - \sum_i x_{NC} - \sum_i x_C\right]} \frac{R}{Na} \ln\left(\frac{I}{I_0}\right)$$

Comparison of methods



Thank you.



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